

NORSAR Scientific Report No. 1-90/91

Semiannual Technical Summary

1 April — 30 September 1990

Kjeller, November 1990

APPROVED FOR PUBLIC RELEASE, DISTRIBUTION UNLIMITED

7.2 Initial results from real-time processing of GERESS array data

Introduction

The GERESS array (Harjes, 1990) represents the most recent addition to the network of regional seismic arrays in Europe. GERESS, which is located in the Bavarian Forest area in southern Germany, has a geometry similar to that of NORESS in southern Norway and ARCESS in northern Norway, but with a slightly enlarged instrument spacing (Fig. 7.2.1). Thus the diameter of GERESS is 4 km, compared to 3 km for the two arrays in Norway.

Real-time data from GERESS are transmitted continuously both to Bochum, Germany (by land line), and to the NORSAR Data Processing Center (NDPC) at Kjeller (by satellite). At NDPC, the data are currently subjected to continuous real-time detection processing, using the RONAPP algorithm (Mykkeltveit and Bungum, 1984). In the near future, these data will also be incorporated into the Intelligent Monitoring System (IMS) (Bache *et al*, 1990).

GERESS real-time processing

The initial processing of GERESS data is conducted at NDPC using a beam set essentially identical to that being used for NORESS and ARCESS data (see Subsection 3.4). Although several modifications will undoubtedly be desirable after more experience is gained, it is still of interest to observe how a "generic" parameter set performs when applied to a regional array in a new geological environment. Below, we give some initial examples from this processing.

Table 7.2.1 shows excerpts from the automatic GERESS phase detection list for day 293 (23 October 1990). For each phase, the detection time, beam number, SNR, phase velocity and azimuth are listed, together with a number of attributes used in further characterization of the detected phase.

In Fig. 7.2.2 we show an automatically generated event plot (Fyen, 1989) for one of the located events during the time period covered by the detection list in Table 7.2.1. This event is located in the Lubin mining district in Poland, at a distance of 344 km from GERESS, and is probably one of a large number of rockbursts known to occur in that region (Gibowics, 1987). We note that this event was too small to be detected by either NORESS, ARCESS or FINESA.

Fig. 7.2.3 shows GERESS automatic output plot from the P-wave detection of the Novaya Zemlya explosion 24 October 1990 ($\Delta = 30.4$ degrees). The phase velocity is indicative of a teleseismic signal, and the estimated azimuth is consistent with the actual epicenter. GERESS SNR is 105 on the array beam, which is naturally lower than for the three other arrays, all of which are within regional distances from Novaya Zemlya. An interesting feature of the GERESS recordings of this event is a very sharp PcP detection at 2 min 59.5 seconds after P (Fig. 7.2.4). The time differential between P and PcP gives a very sharp constraint on the epicentral distance, in particular when the phase onset times can be read as precisely as in this case. Thus, given appropriate calibration, very useful location information could be derived.

Conclusions

Our initial experience shows that real-time processing of GERESS data will form a very valuable contribution to the regional array monitoring research network. So far, it appears that many new events in southern Europe within 500 km distance from GERESS will be added, and GERESS data will provide further constraints on the events detected and located by more than one array. The teleseismic potential of GERESS is also quite promising.

J. Fyen

References

- Bache, T., S.R. Bratt, J. Wang, R.M. Fung, C. Kobryn and J. Given (1990): The Intelligent Monitoring System, Bull. Seism. Soc. Am., Special Issue, in print.
- Fyen, J. (1989): Event processor program package, . Tech. Summary, 1 Oct 1988 - 31 Mar 1989, NORSAR Sci. Rep. No. 2-88/89, Kjeller, Norway.
- Gibowics, S. (1987): NORESS capability for detection and location of mining tremors in the Lubin area in Poland, In: Semiannual Technical Summary, 1 September 1986 – 31 March 1987, NORSAR Sci. Rep. No. 2-86/87, NORSAR, Kjeller, Norway.
- Harjes, H.-P. (1990): Design and siting of a new regional array in central Europe, Bull. Seism. Soc. Am., Special Issue, in print.
- Mykkeltveit, S. and H. Bungum (1984): Processing of regional seismic events using data from small aperture arrays, Bull. Seism. Soc. Am., 74, 2313– 2333.

323 293:12.43.29 700	1.10 G053	4.8	2.6 nois	298.5 0.06 4	4.02	953.3	173.9 A3 sz	-1.00 - 1.00 - 1.00 - 1.00
324 293 12 43 39 750	1 25 GV01	3.8	12.9 P	191.0 0.17 1	0.56	76.5	404.7 C1 sz	0.59 2.06 80.33 4.28
325 293.12 45 10 987	0 31 6084	7.7	2.5 nois	310.0 0.07 4	6.31	2650.3	505.5 D5 sz	-1.00 - 1.00 - 1.00 - 1.00
326 293.12 45 10 200	1 20 GV01	7.2	4.3 S	201.9 0.11 3	0.72	289.1	658.7 D5 sz	-1.00 - 1.00 - 1.00 - 1.00
227 202.12 47 07 050	0 75 C043	15 5	2 4 nois	124 5 0 05 4	3 16	1472 7	268 3 05 57	-1.00 - 1.00 - 1.00 - 1.00
	1 02 0045	2.2	1 0 nois	310 0 0 09 3	1 70	1713 6	609 2 C5 87	-1 00 -1 00 -1 00 -1 00
328 293:12.4/.16.4/5	1.02 GV00	3.4	14 7 0	310.0 0.09 3	1 21	74 5		
329 293:12.47.39.300		1.4	14.7 P	202.0 0.29 1	1.51	110 7	340.9 CJ_32	
330 293:12.56.39.725	0.98 GVUI	0.0	33.9 P	346.7 0.34 1	1.04	110.7	498.4 A3_SZ	
331 293:12.58.45.675	0.22 GH03	3.9	2.9 nois	45.7 0.07 3	1.14	2095.2	299.4 CI_SZ	-1.00 -1.00 -1.00 -1.00
332 293:12.58.50.300	0.50 G032	4.5	37.7 P	14/.3 0.09 3	3.30	167.0	85.9 C1_sz	-1.00 - 1.00 - 1.00 - 1.00
333 293:13.01.31.481	1.12 G103	6.8	2.8 nois	339.3 0.04 4	7.74	2619.1	659.5 A0_sz	0.34 1.85 86.29 33.93
334 293:13.04.21.800	1.30 G034	7.3	2.8 nois	145.4 0.07 3	2.13	477.6	126.0 A3_sz	-1.00 - 1.00 - 1.00 - 1.00
335 293:13.04.27.650	0.65 G021	4.7	3.2 S	3.6 0.05 4	1.94	491.2	118.1 A3_sz	-1.00 - 1.00 - 1.00 - 1.00
336 293:13.11.29.750	0.55 G036	7.3	2.8 nois	140.6 0.08 3	2.14	349.7	134.6 A3 sz	-1.00 - 1.00 - 1.00 - 1.00
337 293 13 11 40.075	1.12 GV01	3.1	15.6 P	30.5 0.56 1	0.79	164.7	335.2 A3 sz	0.60 3.14 88.70 5.40
338 293.13 15 50 331	0.17 GH04	3.7	2.4 nois	31.0 0.05 4	8.29	689.6	256.7 A0 sz	0.19 2.25 64.50 5.08
339 293.13 22 49 575	0.52 6033	4.6	2.8 nois	150.1 0.10 4	2.51	398.6	77.3 D8 sz	-1.00 - 1.00 - 1.00 - 1.00
340 203.13 27 39 625	1 07 GV01	5 6	11 6 P	124.1 0 47 1	0 93	45 0	464 5 A3 SZ	-1 00 -1 00 -1 00 -1 00
241 202.12 27 50 675	1 32 CV01	2.0	100	343 5 0 48 1	0.55	195.0	334 5 B3 67	-1 00 -1 00 -1 00 -1 00
341 293:13.27.39.073	1.12 GV01	3.1	4.0 B		0.04	72 0	220 6 12 64	-1.00 -1.00 -1.00 -1.00
342 293:13.20.19.075		5.0	7.6 Pyn	222 1 0 04 4	5.60	1010 0	329.0 63_82	
343 293:13.30.14.306	0.59 GH04	4.2	3.1 5	333.1 0.04 4	5.64	1212.3	368.4 A3_52	
344 293:13.33.19.525	1.27 G034	1/./	8.0 Pgn	130.7 0.39 1	2.60	315.0	260.1 A0_sz	0.75 0.50 45.92 75.59
345 293:13.33.29.425	1.17 G044	6.3	8.0 Pgn	150.7 0.40 1	2.95	646.6	300.4 A0_sz	-1.00 - 1.00 - 1.00 - 1.00
346 293:13.36.05.362	0.44 G087	11.2	4.2 S	106.5 0.06 4	6.44	2133.4	697.2 A3_sz	-1.00 - 1.00 - 1.00 - 1.00
347 293:13.36.15.700	1.10 G051	4.9	3.0 nois	149.1 0.06 4	3.88	971.7	137.3 A3_sz	0.16 0.80 65.16 87.88
348 293:14.18.12.350	0.95 G059	12.1	7.5 Pgn	352.9 0.19 1	2.82	643.5	190.8 A0_sz	0.73 0.90 47.35 54.70
349 293:14.18.34.725	1.38 G065	8.9	4.2 SN	354.6 0.14 3	3.25	1872.5	308.1 A0 sz	0.67 1.82 85.96 10.60
350 293:14.18.38.950	1.25 GV06	4.4	4.3 S	0.7 0.12 3	3.93	1300.8	691.4 A0 sz	-1.00 - 1.00 - 1.00 - 1.00
351 293:14.25.06.875	0.92 G044	9.4	3.0 S	142.7 0.06 3	3.05	861.0	197.0 D2 sz	-1.00 - 1.00 - 1.00 - 1.00
352 293:14.25.10.025	1.67 GY02	4.4	2.7 nois	149.5 0.06 3	1.86	406.4	279.0 D2 sz	-1.00 - 1.00 - 1.00 - 1.00
353 293.14 25 36 925	1 38 6055	6 1	2 5 nois	267.7 0.06 4	4.18	645.3	128 0 D7 se	0.20 1 14 78 45 51.94
354 293.14 46 24 550	1 95 GV02	3 1	28 4 P	106 1 0 16 3	1 89	34 9	93 3 B3 SZ	-1 00 -1 00 -1 00 -1 00
355 293.14 49 39 275	1 02 6058	5 6	3 2 5	167 3 0 06 3	3 47	472 1	95 7 43 57	
256 202.14 50 26 100	1 20 0024	5.0	2.25	220 4 0 06 4	2.46	250 0	77 7 02 67	-1.00 -1.00 $+1.00$ -1.00
257 202.14 51 20 250	1.20 G034	4.0	3.0 3 7 0 Dam	164 6 0 20 1	2.40	339.0	572 0 05 an	
357 293:14.J1.39.330		/.4	7.2 Pyll	104.0 0.30 1	0.45	50.4	J72.0 CJ_SZ	
358 293:14.53.21.975	0.82 6051	5.0	1.8 nois	220.2 0.07 4	3.96	400.9	92.2 C1_52	0.17 1.21 12.27 33.70
359 293:14.54.31.281	0.82 G104	/.4	3.2 SN	160.4 0.04 4	8.96	3/40.4	1052.4 A3_sz	0.27 2.95 89.00 4.00
360 293:14.55.49.975	0.62 G035	6.9	2.9 nois	2/4.0 0.05 4	2.69	537.3	110.2 D2_sz	-1.00 - 1.00 - 1.00 - 1.00
361 293:14.57.11.050	1.05 G035	8.2	2.8 nois	140.7 0.07 3	1.98	713.8	133.3 C5_sz	-1.00 - 1.00 - 1.00 - 1.00
362 293:14.57.19.325	1.48 G035	9.9	2.9 nois	153.5 0.05 3	2.15	881.3	225.2 C5_sz	-1.00 - 1.00 - 1.00 - 1.00
363 293:14.57.24.750	0.95 GV02	3.6	2.9 nois	62.5 0.07 3	1.59	391.9	374.2 C5_sz	-1.00 - 1.00 - 1.00 - 1.00
364 293:14.57.52.125	0.88 GV02	3.0	3.0 S	326.0 0.10 4	1.55	179.4	246.1 D5 sz	-1.00 - 1.00 - 1.00 - 1.00
365 293:15.01.53.150	0.95 G034	5.3	3.0 S	153.8 0.08 3	2.18	383.9	79.6 A3 sz	-1.00 - 1.00 - 1.00 - 1.00
366 293:15.07.29.725	0.88 G035	8.7	2.7 nois	284.7 0.05 4	2.47	846.6	144.6 D2 sz	0.35 1.61 82.97 53.64
367 293:15.09.02.475	1.12 G049	5.6	3.8 S	341.7 0.07 3	3.17	416.6	103.9 A3 52	-1.00 - 1.00 - 1.00 - 1.00
368 293 15 11 04 450	0 65 6042	5.1	3.1.5	254.3 0.05 4	2.82	1218.1	103 7 A3 SZ	-1.00 - 1.00 - 1.00 - 1.00
369 293.15 11 31 775	0.82 6056	6 6	35 3 D	223 5 0 06 4	3 84	118 4	170 2 43 57	0 30 1 61 87 77 22 09
270 202.15 18 24 575	0.52 0030	6.0	2.2 5		2.04	762 9		
370 373:1J.10.34.373	1 07 0050	0.0	2.0 1015		4 50	617 0	1475 D5 cr	0.20 0.11 03.04 13.21
371 293:13.10.39.223	1.07 6052	7.7.5	2.0 nois	T02-2 0-03 4	4.39	04/.0	11005 5 00 SZ	
3/2 293:13.43.33.5/5	0.52 G033	101.5	2.4 nois	293.2 0.03 4	2.20	20191.2	LIZZO.O AJ_SZ	
3/3 293:10.08.43.925	2.1/ G011	4.5	6.9 Pgn	348.1 0.19 3	T.08	320.3	183.4 D9_SZ	0.39 2.50 89.11 21.66
3/4 293:16.12.06.075	1.23 G036	5.1	12.4 P	258.1 0.09 4	2.32	122.2	99.8 D8_sz	-1.00 - 1.00 - 1.00 - 1.00
375 293:16.28.21.575	0.52 G049	4.8	2.9 nois	146.9 0.13 3	2.51	343.0	87.3 D5_sz	0.57 0.87 39.37 48.97
376 293:16.28.25.875	2.12 GV06	5.3	6.8 Pgn	33.3 0.19 3	4.82	880.2	566.5 D5_sz	0.59 0.94 41.68 50.28
377 293:16.28.35.800	0.50 G057	4.8	6.8 Pgn	32.3 0.21 2	3.71	417.6	147.1 D5_sz	-1.00 -1.00 -1.00 -1.00
378 293:16.29.10.675	0.52 GH01	6.2	4.6 S	40.1 0.20 3	2.88	2349.6	1100.9 B3 sz	0.22 1.45 71.53 14.51

•

· · · ·

Table 7.2.1. (Page 1 of 2)

379 293:16.29.14.425	1.57 GV02	4.0	3.3 LG	31.5 0.31 2	1.47	1019.1	508.0 B3 sz	0.55 1.41 79.68 77.38
380 293:16.29.18.375	1.62 GV02	3.1	4.4 S	24.5 0.32 1	1.59	1159.0	505.8 B3 sz	-1.00 - 1.00 - 1.00 - 1.00
381 293:16.29.19.725	0.98 GV01	5.6	3.5 S	19.1 0.23 2	1.51	764.1	915.5 A0 sz	-1.00 - 1.00 - 1.00 - 1.00
382 293:16.35.18.525	2.48 GV01	3.4	29.9 P	277.5 0.14 3	0.83	114.9	304.4 D4 sn	-1.00 - 1.00 - 1.00 - 1.00
383 293:17.12.59.500	1.20 GV01	5.6	26.4 P	146.9 0.45 1	1.08	158.6	681.5 B3 sz	-1.00 - 1.00 - 1.00 - 1.00
384 293:17.15.23.700	0.90 G093	7.1	6.3 Pqn	113.5 0.05 4	7.43	1175.0	453.0 A3 sz	-1.00 - 1.00 - 1.00 - 1.00
385 293:17.36.39.750	0.95 GV01	7.6	5.0 S	206.3 0.14 4	1.03	286.6	902.8 B2 sz	-1.00 - 1.00 - 1.00 - 1.00
386 293:17.48.42.350	0.95 G049	5.3	4.4 S	145.0 0.06 3	3.27	506.9	100.5 A3 sz	-1.00 - 1.00 - 1.00 - 1.00
387 293:17.51.19.950	0.75 GV01	6.0	9.4 Pan	315.4 0.24 1	0.57	94.2	460.0 A0 sz	-1.00 - 1.00 - 1.00 - 1.00
388 293:18.38.37.850	3.15 GV01	3.4	8.2 Pgn	187.5 0.42 1	0.86	44.2	400.8 C1 sz	0.25 1.78 88.86 8.36
389 293:18.46.16.650	1.45 G042	4.9	2.9 nois	138.2 0.14 3	3.05	597.5	88.7 B5 sz	-1.00 - 1.00 - 1.00 - 1.00
390 293:18.48.49.825	0.48 G071	5.0	3.3 S	121.9 0.05 4	4.77	435.7	166.8 A3 sz	-1.00 - 1.00 - 1.00 - 1.00
391 293:18.49.08.950	1.55 GV04	3.1	2.7 nois	140.1 0.08 3	2.37	294.5	212.6 C5 sz	-1.00 - 1.00 - 1.00 - 1.00
392 293:18.49.19.525	0.77 G054	5.2	13.0 P	290.4 0.06 4	4.01	86.6	103.2 D5 sz	-1.00 - 1.00 - 1.00 - 1.00
393 293:18.51.32.550	1.55 G053	5.6	2.8 nois	321.8 0.07 4	3.68	521.0	101.3 A0 sz	0.54 2.47 85.13 18.21
394 293:18.56.19.125	1.57 GV01	4.0	4.8 S	294.2 0.16 3	1.02	369.7	423.5 D2 sz	-1.00 - 1.00 - 1.00 - 1.00
395 293:19.08.01.150	1.55 GY02	3.1	2.2 nois	129.2 0.08 3	1.68	283.3	186.2 D2 sz	-1.00 - 1.00 - 1.00 - 1.00
396 293:19.08.39.500	1.20 GV01	6.4	8.3 Pan	162.1 0.42 1	0.63	130.4	774.7 D5 sz	-1.00 - 1.00 - 1.00 - 1.00
397 293:19.10.00.175	0.82 GV01	3.8	5.8 S	23.0 0.32 1	0.64	251.0	385.7 B4 sz	-1.00 - 1.00 - 1.00 - 1.00
398 293:19.19.29.750	0.55 G021	4.6	16.4 P	132.7 0.06 4	1.98	176.5	102.9 A3 sz	-1.00 - 1.00 - 1.00 - 1.00
399 293:19.21.18.775	2.42 GV01	3.3	5.8 S	185.7 0.29 1	0.87	324.8	368.5 D8 sz	-1.00 - 1.00 - 1.00 - 1.00
400 293:19.31.39.900	1.10 GV01	3.9	7.1 Pgn	167.2 0.26 1	0.85	64.1	377.5 D2 sz	-1.00 - 1.00 - 1.00 - 1.00
401 293:19.40.59.925	1.07 GV01	3.3	22.8 P	14.2 0.44 1	0.93	65.9	314.0 A3 sz	1-1.00 -1.00 -1.00 -1.00
402 293:19.48.59.775	0.92 GV02	4.0	2.2 nois	29.2 0.08 3	1.97	211.5	213.5 C1 sz	-1.00 - 1.00 - 1.00 - 1.00
403 293:20.07.57.375	2.92 G011	5.1	34.3 P	310.0 0.17 3	1.06	241.5	234.1 D2_sz	-1.00 - 1.00 - 1.00 - 1.00
404 293:20.10.40.450	0.55 GV05	3.3	2.9 nois	146.0 0.13 3	2.16	285.6	256.6 C1_sz	-1.00 - 1.00 - 1.00 - 1.00
405 293:20.18.48.525	0.77 G065	5.0	2.1 nois	218.7 0.06 4	4.11	363.7	89.4 D7 <u>s</u> n	-1.00 - 1.00 - 1.00 - 1.00
406 293:20.20.40.025	0.98 GV02	3.0	6.1 Pgn	359.9 0.08 4	1.79	55.2	173.2 D9_sz	0.27 1.47 85.01 40.82
407 293:20.51.39.850	0.75 G053	4.8	3.2 SN	266.1 0.06 3	3.93	252.0	57.4 D2_sz	0.28 1.81 86.86 14.22
408 293:21.08.19.750	1.25 GV01	3.6	16.4 P	179.1 0.53 1	0.57	135.1	387.1 D8_sz	-1.00 - 1.00 - 1.00 - 1.00
409 293:21.15.19.675	1.32 GV01	3.4	13.8 P	228.6 0.15 3	0.48	63.1	325.8 D5 <u>s</u> z	-1.00 - 1.00 - 1.00 - 1.00
410 293:21.27.39.925	1.07 GV01	4.2	12.1 P	278.5 0.32 3	0.88	170.9	317.6 A3 <u>s</u> z	0.28 2.03 84.67 15.54
411 293:22.09.09.175	2.62 G021	5.1	48.6 P	329.0 0.32 2	1.33	179.7	110.9 A0 <u>s</u> z	-1.00 - 1.00 - 1.00 - 1.00
412 293:22.40.00.225	0.77 GV01	4.0	4.8 S	317.6 0.33 1	0.96	229.5	341.6 B3 <u></u> sz	-1.00 - 1.00 - 1.00 - 1.00
413 293:23.17.59.375	1.62 GV01	3.1	8.8 Pgn	227.4 0.37 1	0.96	82.7	237.1 D5 <u></u> sz	-1.00 - 1.00 - 1.00 - 1.00
414 293:23.21.19.750	1.25 GV01	3.2	4.6 S	315.9 0.49 1	0.75	203.8	242.9 A3_sz	-1.00 - 1.00 - 1.00 - 1.00
415 293:23.49.17.775	3.23 GV01	3.2	10.4 P	85.5 0.10 3	0.86	65.2	326.6 D9_sz	-1.00 - 1.00 - 1.00 - 1.00

Table 7.2.1. Automatic event processor detection log for the GERESS array. From left to right the columns give arrival identification number, estimated onset time, difference in seconds between STA/LTA trigger time and onset time, beam name, SNR, velocity in km/sec, phase name, azimuth, broadband FK relative coherence measure and quality of FK (1=good), frequency in Hz of estimated maximum amplitude of the phase, phase maximum amplitude in uncorrected digital counts, STA. The next column with channel names gives, in case of many data gaps, the name of one channel that due to gaps/spikes, etc., may have contributed to a false detection. The four last numbers are result of three-component polarization analysis, and give rectilinearity, horizontal/vertical ratio, angle of incidence 1 and 3. (Page 2 of 2)

11.0



Fig. 7.2.1. Geographical location and geometry of the GERESS array in Germany (after Harjes, 1990).

.

EPX 190 1990 FKX 376 Phos	0-293:1 se PN of	6.27.35.996 Lat	51.40 Lon 16.37 Azi 32.56 Dst 344.31 A 1282.0 , 1282.0 f 1.47 ML 3.9 8.25.875 vel 6.80 azi 33.30 rpw 0.190 g 3 g 1282.0 f 4.82 fbgnd 3.50	91 5.50
GER_AO_sz			ljänjardenin alphännisisse henanissen avar det bridenn socialisisen i varar den det andere värade alsadaratele värade operate operate operate	13193.
GER_B1_sz	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	Abda - Abda have hill have	h	1785.2
GER.B2.sz	e halan da sana ar a			2092.5
GER_B3_sz				10456.
GER_B4_sz			n na star an	1960.6
GER_B5_sz	(847-14 ¹ -14) (11)		🚓 🖗 🖶 markan sun ikan isan isan kara sa kara sa kara sana da akar sa kara ta kara na sanakan kara sa kara na kara	3207.2
GER_C1_sz	***		afa junta annanta' ha la baatan na mannaan dha na mar an an an annan ann hainn an an ha an an an an an an an an An annan	1961.5
GER_C2_sz	he la staat t		hetweinen in hit der versten der Brest frieden stellten die gestellten aus einen der verstellten ander beiterten er verstellten der	1882.0
GER_C3_sz			######################################	3205.2
GER_C4_sz	Hereit in the second		🗱 🕹 General Manufer in the State of Cale of State Cale o	2284.7
GER_C5_sz	***		•	2133.5
GER_C6_sz	•••••		## ##################################	2514.3
GER_C7_sz		and the of the particular of t	*** *********************************	1733.3
GV06	++++++++	half an arrest the state		1385.4
GV02				835.86
GERESS	199	90-293:1 <u>6.27.5</u>	55.875 20/10/90 17:44:5	8 NORSAR

Fig. 7.2.2. Automatically generated event plot for GERESS. The traces shown are a selection of single instruments filtered in the band 3.5-5.5 Hz. The bottom two traces are the P- and S-beams using the velocities and azimuths determined by broadband F-K analysis. (The S-beam, which is the lowermost trace, is filtered in the band 1.0-2.0 Hz). The time window is 6 minutes.

FKX 1388 be Phase P vel	2m G032 At 1990-297:15.04.13.725 snr 105.20 19.70 azi 42.30 rpw 0.510 q 1 a 3792.1 f 2.28	,fband 1.50 3.50	
050 40			7078.8
GERAUSZ			/930.0
GER_C4_sz		-WWWWWWWWWWWWWWWWWWWWW	6621.4
GER_C5_sz		-MMM/how www.www.when.www.when.	9848.3
GER_C6_sz	······································	MMMmmmmmmmmmmmmmmmmmmmmmmmmmmmmmmmmmmmm	8522.4
GER_C7_sz		MMM www.www.www.www.www.www.	7619.5
GER_D1_sz			8230.3
GER_D2_sz		MMM Manna Manna Markan Marka	8704.8
GER_D3_sz		-MMM/mmmmmmmmmmmmmmmmmmmmmmmmmmmmmmmmmm	8398.5
GER_D4_sz		MMM Marken Mar	7701.4
GER_D5_sz		- MMM	7103.7
GER_D6.sz		MMMMMMMMMMMMMMMMMMMMMMMMMMMMMMMMMMMMMMM	7863.1
GER_D7_sz		MMMmmmmmmmmmmmmmmmmmmmmmmmmmmmmmmmmmmmm	8193.5
GER_D8_sz		MMMMMMMMMMMMMMMMMMMMMMMMMMMMMMMMMMMMMMM	8310.8
GER_D9_sz		MMM/mmmmmmmmmmmmmmmmmmmmmmmmmmmmmmmmmm	7287.9
G032	· · ·	MMM mannen mannen	7565.7
G032		MMuphaman	10866.
	04.00	04.20 04.40	
GERESS	1990-297:15.03.43.725	25/10/90 03:43:-	45 NORSAR

Fig. 7.2.3. Automatically generated teleseismic phase plot for GERESS, corresponding to the P-wave detection of the Novaya Zemlya explosion on 24 October 1990. The traces shown are a selection of single instruments filtered in the band 1.5–3.5 Hz. The bottom two traces are the P-beam filtered and unfiltered, using the velocity and azimuth determined by broadband FK analysis. The time window is 60 seconds.

EKY 1300 ha	am CO31 At 1990-29715 07 13 225 ppr 16 0					
Phase P vel	41.50 azi 17.70 rpw 0.560 a 1 a 3792.1 f 1.97 fband 1.50 3.50					
<u></u>	┧╷╴╷╴╷╷╷╷╷╷╴╷╴╷╴╷╴╷╴╷╴╷╴╎╴╷ <mark>┤</mark> ┣╶╷╴╷╴╿╴╷╴╷╴╷╴╷╴╷╴╷╶╷╶┤╶╷┤					
GER_A0_sz	- Marken Marke	4391.7				
GER_C4_sz		3451.5				
GER_C5_sz	-www.mar.www.mar.www.mar.www.www.www.www.www.www.	4367.3				
GER_C6_sz	firm www.www.www.www.www.www.www.www.www.ww	4199.6				
GER_C7_sz	f. www.www.www.www.www.www.www.www.www.w	4095.2				
GER_D1_sz	-manus manus manus Manus manus manus	4007.0				
GER_D2_sz	for the second s	3786.5				
GER_D3_sz	-www.www.www.www.www.www.www.www.www.ww	4176.5				
GER_D4_sz		3962.9				
GER_D5_sz		2531.6				
GER_D6_sz	-www.www.www.www.www.www.www.www.www.ww	3062.3				
GER_D7_sz		3905.6				
GER_D8_sz	f.	5626.4				
GER_D9_sz	f	4004.3				
G031		3792.1				
G031		6059.8				
ICERESS 1990-297:15.06.43.225 25./10/00.03:62:33						
<u></u>		a nononn				

Fig. 7.2.4. Similar to Fig. 7.2.3, but showing the automatic plot for the PcP phase of the Novaya Zemlya explosion. Note the clear onset and the significant noise suppression on the filtered beam (second trace from bottom). Also note that the high estimated phase velocity (41.50 km/s) is a clear indication that this is indeed a core phase.