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Semiannual Technical Summary

1 April — 30 September 1990

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Abstract

This Semiannual Technical Summary describes the operation, maintenance and research activities at the Norwegian Seismic Array (NORSAR), the Norwegian Regional Seismic Array (NORESS) and the Arctic Regional Seismic Array (ARCESS) for the period 1 April – 30 September 1990. Statistics are also presented for additional seismic stations, which through cooperative agreements with institutions in the host countries provide continuous data to the NORSAR Data Processing Center (NPDC). These stations comprise the Finnish Experimental Seismic Array (FINESA), the German Experimental Seismic Array (GERESS), and from the fall of 1990, two 3-component station in Poland: Ksiaz and Stary Folwark. This Semiannual Report also presents statistics from operation of the Intelligent Monitoring System (IMS). The IMS has been operated in an experimental mode using NORESS and ARCESS data, and the performance has been very satisfactory.

The NORSAR Detection Processing system has been operated throughout the period with an average uptime of 98.0% as compared to 91.8% for the previous reporting period. A total of 2359 seismic events have been reported in the NORSAR monthly seismic bulletin. The performance of the continuous alarm system and the automatic bulletin transfer by telex to AFTAC has been satisfactory. A system for direct retrieval of NORSAR waveform data through an X.25 connection has been implemented, and has been tested successfully for acquiring such data by AFTAC. Processing of requests for full NORSAR/NORESS data on magnetic tapes has progressed according to established schedules.

On-line detection processing and data recording at the NORSAR Data Processing Center (NDPC) of NORESS, ARCESS and FINESA data have been conducted throughout the period, with an average uptime of 92.9% for NORESS and 95.6% for ARCESS. The field computer at the FINESA array was damaged by a thunderstorm in May, and FINESA was out of operation until the end of August. The Intelligent Monitoring System was installed at NORSAR in December 1989 and has been operated experimentally since 1 January 1990. Results of the IMS analysis for the reporting period are given.

There have been no modifications made to the NORSAR data acquisition system. The process of evaluating technical options for upgrading the array is continuing. A test of a full subarray acquisition system will be performed during the next reporting period.

The routine detection processing of NORESS, ARCESS and FINESA is running satisfactorily on each of the arrays' SUN-3/280 data acquisition systems. The routine processing of FINESA data at NORSAR is similar to what is done in Helsinki. GERESS data acquisition and detection processing has commenced during the period. Maintenance activities in the period comprise preventive/corrective maintenance in connection with all the NORSAR subarrays, NORESS and ARCESS. In addition, the maintenance center has been involved with modification of equipment for FINESA and preparatory work in connection with NORESS HF instrumentation. Other activities involved testing of the NORSAR communications systems.

We have continued our work aimed at evaluating the stability of RMS Lg for yield estimation purposes. Using yield data which have recently become available in a Soviet publication, we have found that NORSAR RMS Lg correlates significantly better with yield than does world-wide m_b . These same yield data have been used to evaluate the NORESS detection threshold for Semipalatinsk explosions, and the 90 per cent threshold in terms of yield is found to be as low as 0.1 kt. This low threshold assumes that the explosion is fully coupled and that the background noise is at a normal level.

An initial assessment of results from real-time processing of GERESS array data has been conducted. We have found that a "generic" beam deployment, identical to that in use at NORESS and ARCESS, also works well for the GERESS array. As more experience is gained, we expect, however, that some of the special signal and noise characteristics at the GERESS site will make it desirable to modify some parameters in order to optimize detection performance. So far, GERESS detects a number of earthquake and man-made explosions within 500 km which are not detected by other regional array stations. It also provides additional information which will improve the location accuracy for events detected by multiple stations in the regional network.

The generalized beamforming technique developed by Ringdal and Kværna is now being applied to the network of 4 regional arrays (NORESS, ARCESS, FINESA, GERESS). Initial experience has confirmed the effectiveness of this method in automatically and rapidly providing initial phase associations and epicenter estimates for regional events. For a five-day test period, several hundred regional events were associated, most of which were detected by one array only (P and Lg phases). A total of 37 events had 4 or more phase detections by the regional network. Analyst inspection revealed that 36 of these were properly associated and located, whereas one represented a coincidental match of unrelated phase detections. Further work is now being conducted to fine tune the parameters used by this method, and also to consider incorporating a dynamic consistency check using the thresholds computed by the threshold monitoring technique to assess the likelihood of phase associations.

The concept of threshold monitoring, introduced by Ringdal and Kværna, is a method of monitoring the seismic amplitude levels for the purpose of using this information to assess the largest size of events that might go undetected by a given network. In an effort to demonstrate the capabilities of this threshold monitoring concept, a preliminary version has been implemented into the Intelligent Monitoring System (IMS). Using recordings by the NORESS, ARCESS and FINESA arrays, the method has been applied for monitoring continuously the Novaya Zemlya test site for a full one-week period. It is demonstrated that the implementation of the threshold monitoring method in the IMS system enables real-time operation. The displays provided by the threshold monitor are particularly valuable in pointing out time intervals of special interest, thus aiding the analyst in his work. The interesting intervals can then be examined by different processing techniques to locate and identify the events. In the actual one-week monitoring experiment, we have found that the combined three-array threshold for Novaya Zemlya is $m_b = 2.2$ or lower 50 % of the time, and $m_b = 2.5$ or lower 99 % of the time. All instances where the threshold exceeds $m_b = 2.5$ correspond to actual interfering seismic events, either regional or teleseismic. Methods are currently being studied on how to further analyze the data during such interference, with the aim to establish operationally reliable monitoring at the lowest possible threshold.

The concept of a very small "hybrid" array/3-component station has been studied. We have used the NORESS A-ring subarray as a test station for a one-week on-line detection processing experiment. We have found that this small array, which has a diameter of only 300 m (i.e., 1/10 of that of NORESS) has a remarkably good performance in distinguishing P and S phases (based on phase velocity estimates) and in obtaining useful azimuth estimates for all phase types. Thus it would appear that supplementing 3-component stations with small triangular arrays of the A-ring type would to a large extent alleviate the problems now encountered in 3-component analysis of secondary phases.

Work is proceeding toward establishing two modern 3-component stations in Poland (Ksiaz and Stary Folwark) with continuous data transmission by satellite to NDPC for integration into the IMS processing. An initial report on the system design, including site descriptions, communication arrangements and the NDPC data acquisition system is presented. An example of data recorded at Ksiaz indicates that data from this station are of high quality and will give a valuable contribution to the regional station network.

Further work on statistically optimal array detection, using a generalization of Capon's maximum likelihood technique, is reported. Examples are presented both for array detection and onset time estimation of regional and teleseismic phases. It is shown in particular that the very strong, low frequent microseismic noise observed at NORESS and ARCESS can be effectively suppressed, due to the high noise coherency. Thus it is possible to regenerate signal waveforms for which the signal is represented in an undistorted way, whereas the microseismic noise is suppressed by as much as 12–18 dB.

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1 Summary

This Semiannual Technical Summary describes the operation, maintenance and research activities at the Norwegian Seismic Array (NORSAR), the Norwegian Regional Seismic Array (NORESS) and the Arctic Regional Seismic Array (ARCESS) for the period 1 April – 30 September 1990. Statistics are also presented for additional seismic stations, which through cooperative agreements with institutions in the host countries provide continuous data to the NORSAR Data Processing Center (NPDC). These stations comprise the Finnish Experimental Seismic Array (FINESA), the German Experimental Seismic Array (GERESS), and from the fall of 1990, two 3-component station in Poland: Ksiaz and Stary Folwark. This Semiannual Report also presents statistics from operation of the Intelligent Monitoring System (IMS). The IMS has been operated in an experimental mode using NORESS and ARCESS data, and the performance has been very satisfactory.

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The research activity is summarized in Section 7. Section 7.1 presents a continuation of the evaluation of the stability of RMS Lg for yield estimation purposes. Initial results from real-time processing of GERESS array data are given in Section 7.2. In Section 7.3 a study of generalized beamforming using a network of regional arrays is presented. The continuous threshold monitoring technique as applied to the Novaya Zemlya test site is discussed in Section 7.4. Section 7.5 discusses real-time processing using data from a hybrid 3-component/small array station. In Section 7.6 development work, including system design, site descriptions, communication arrangements and the NDPC data acquisition system, in connection with two new three-component stations in Poland is presented. Optimal group filtering and noise attenuation for the NORESS and ARCESS arrays is discussed in Section 7.7.

2 NORSAR Operation

2.1 Detection Processor (DP) operation

There have been 55 breaks in the otherwise continuous operation of the NOR-SAR online system within the current 6-month reporting interval. The uptime percentage for the period is 98.0 as compared to 91.8 for the previous period.

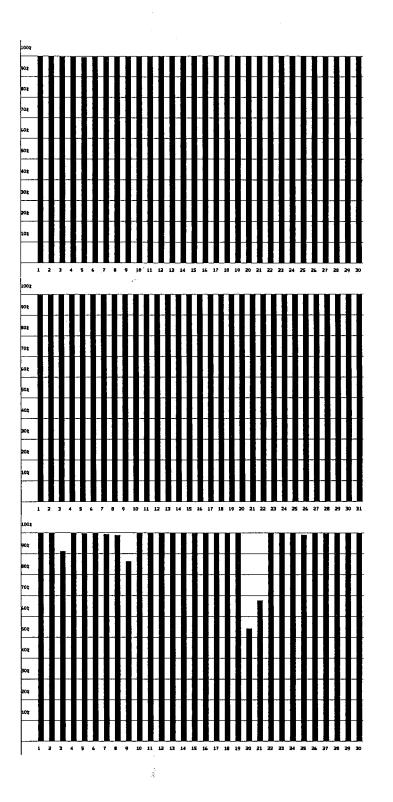
Fig. 2.1.1 and the accompanying Table 2.1.1 both show the daily DP downtime for the days between 1 April and 30 September 1990. The monthly recording times and percentages are given in Table 2.1.2.

The breaks can be grouped as follows:

a)	Hardware failure	12
b)	Stops related to program work or error	4
c)	Hardware maintenance stops	2
d)	Power jumps and breaks	3
e)	TOD error correction	10
f)	Communication lines	24

The total downtime for the period was 87 hours and 11 minutes. The mean-time-between-failures (MTBF) was 3.2 days, as compared to 1.6 for the previous period.

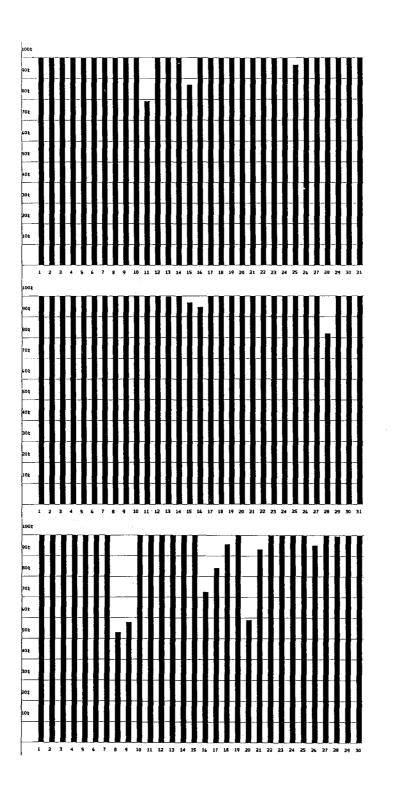
J. Torstveit



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Fig. 2.1.1 Detection Processor downtime for April (top), May (middle) and June (bottom) 1990.



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Fig. 2.1.1 Detection Processor downtime for July (top), August (middle) and September (bottom) 1990.

LIS	r of Bi Stài	REAKS	IN DP STOP	PR	CESSING THE LAST COMMENTS
DAY	STA	KT.	510F		COMMENTS
92	5	40	5	42	TOD RETARED 14MS
93	4	57	5	0	TOD RETARED 7MS
95	7	59	8	6	TOD ADJUSTMENT
107	6	0	6	2	TOD RETARED 27MS
113	6	14	6	16	TOD RETARED 13MS
116	12	35	12 12	37 2	TOD RETARED 40MS TOD RETARED 12 S
$122 \\ 154$	12 6	0 14	8	19	TOD RETARED 12 S CPU FAILURE
156	6	54	6	57	TOD RETARED 7MS
158	· 6	10	ĕ	14	LINE FAILURE
158	11	$\overline{24}$	11	28	LINE FAILURE
159	8	45	8	48	LINE FAILURE
159	9	2	9	7	LINE FAILURE
159	9	37	9	40	LINE FAILURE
159	9	58	10	.0	LINE FAILURE
159	12	12	12	14	LINE FAILURE
160	18 9	21 16	21 9	36 19	AIRCOND. FAILURE LINE FAILURE
166 171	13	0	24	0	LINE FAILURE
172	13	ŏ	7	44	LINE FAILURE
176	12	8 8	12	22	CE MAINTENANC
178	6	31	6	34	TOD RETARED 31MS
184	5	42	5	43	LINE FAILURE
184	10	53 28	10	54 29	LINE FAILURE
185	10		10	29	LINE FAILURE
185	10	34	10	35	LINE FAILURE
187	11	29	11	30	LINE FAILURE
192	6 16	28 35	11 19	27 42	MODCOMP FAILURE AIRCOND. FAILURE
196 199	10	48	11	50	LINE FAILURE
200	12	25	12	27	LINE FAILURE
201	10	18	10	20	LINE FAILURE
206	- Ř	30	_ <u>9</u>	19	POWER FAILURE
225	6	48	6	50	LINE FAILURE
225	11	55	11	57	LINE FAILURE
227	11	2	12	47	DP-ONLINE TEST
228	10	7	11	20	DP-ONLINE TEST
228	11	32	11	34 25	LINE FAILURE
232 239	6 10	23 45	6 10	25 47	LINE FAILURE LINE FAILURE
239	10	30	4	40	POWER BREAKE
240	6	27	6	30	LINE FAILURE
240	Ğ	34	7	38	POWER BREAKE
249	6	Ō	6	2	TOD RETARED 8MS
251	12	43	24	0	SOFTWARE PROBLEM
252	0	0	10	6	SOFTWARE PROBLEM
259	5	49	12	25	HARDWARE FAILURE
260	2	49	6	36	HARDWARE FAILURE
261	2	45	3	45	HARDWARE FAILURE
261	5	38	5	40 20	LINE FAILURE
263 263	0 13	18 43	5 18	20	SOFTWARE PROBLEM MAINTENANCE POWER
263	13	43 15	19	45	HARDWARE FAILURE
264	12	15	12	15	HARDWARE FAILURE
264	21	59	23	22	HARDWARE FAILURE
269	19	25	20	33	HARDWARE FAILURE
271	13	18	13	25	HARDWARE FAILURE

HALF-YEAR

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Table 2.1.1 Daily DP downtime in the period 1 April - 30 September 1990.

Month	DP Uptime	DP Uptime	No. of	No. of Days	DP MTBF*
	Hours	%	DP Breaks	with Breaks	(days)
APR 90	719.72	99.96	6	6	4.3
MAY 90	743.97	100.00	1	1	
JUN 90	695.17	96.55	14	10	1.9
JUL 90	743.92	98.88	11	9	2.6
AUG 90	736.58	99.00	10	6	2.8
SEP 90	674.50	93.68	13	10	2.0
		98.03	55	42	3.2

*Mean-time-between-failures = total uptime/no. of up intervals.

Table 2.1.2 Online system performance, 1 April – 30 September 1990.

2.2 Array communications

General

Table 2.2.1 reflects the performance of the communications system throughout the reporting period.

April and May were good months regarding the communications systems. 02C failed due to loss of power, and 06C had problems due to an irregularity related to the CTV equipment.

June was characterized by unstable line conditions affecting all the subarrays, but also subarray electronics failed (02B) and a communication cable between Berger central and the CTV (04C) failed.

In July 02B lost power (week 28), 03C lost synchronization frequently (week 28), and 06C was down approximately 8 hours (week 27) in connection with loss of synchronization after TOD adjustment.

In August 4 subarrays were affected: 02B (weeks 33,34) caused by lightning and loss of power; 02C (week 33) due to an unknown cause; 04C also in connection with lightning and loss of power; 06C was interrupted 11 August, also due to an unknown reason and resumed operation 13 August after a Modcomp restart.

September was also a good period with regard to the communications systems. Only 02B was affected, experiencing spikes on SP channel 04. As previously stated in our reports, the TOD (Time of Day Generator) is less reliable than before, and will probably soon be replaced with by a new system.

Detailed summary

April (weeks 14-17), 2-29.4.90

02C was down from 28 April due to loss of power.

May (weeks 18-22), 30.4-3.6.90

As stated above 02C was affected by loss of power (week 22) and 06C was affected by an irregularity related to the CTV equipment (weeks 20, 21 and 22).

June (weeks 23-26), 4.6-1.7.90

In June all the subarray communications systems were affected by the NTA transmission system (20-21 June). In addition, individual subarrays were also affected: 02B by power outage and SLEM failure (weeks 23, 24 and 25) and 02C (weeks 23, 24) by power failure. Also 04C continued to fail in connection

with a bad cable section between Berger central and the CTV.

July (weeks 27-30), 2-29.7.90

02B, which is in an exposed position with respect to wind, lightning and snow conditions, again failed (9-16 July) due to loss of power. Afterwards NMC Hamar had to reset the SLEM. 03C was affected 4, 10-11 July by excessive resynchronization attempts.

The 04C communications problems, where NTA, NMC and NDPC were involved, were brought to an end 10 July. The next two weeks of the period the communications system operated well. 06C was affected 4 July for approximately 8 hours as a cable between Løten and the subarray was cut by an excavator.

August (weeks 31-35), 30.7-2.9.90

02B was affected 15 and 17 August by lightning and loss of power. In both cases visits to the subarray were necessary to restore the SLEM operation.

18 and 20 August 02C went down, reason not found. After Modcomp restart, the system resumed operation.

Also 04C was affected by lightning and power loss 9 and 16 August.

06C was interrupted 11 August due to an unknown cause. After a Modcomp restart 13 August, the system resumed operation.

September (weeks 36-39), 3-30.9.90

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In September all communications systems functioned satisfactorily. 02B was affected between 22 and 24 September probably under the influence of spikes on SP channel 4.

O.A. Hansen

Sub-	Apr 90 (4)	May 90 (5)	Jun 90 (4)	Jul 90 (4)	Aug 90 (5)	Sep 90 (4)	Average
arrays	2-29.4	30.4-3.6	4.6-1.7	2-29.7	30.7-2.9	3-30.9	1/2 year
01A	0.0020	0.0030	²⁾ *0.002	0.002	0.012	0.003	0.004
01B	0.0060	0.0050	³⁾ *0.004	0.009	0.003	0.012	0.006
02B	0.0020	0.0040	4)*N/A	⁹⁾ *0.003	13)*0.002	¹⁷⁾ *0.014	$^{18)}0.005$
02C	0.0009	0.0020	⁵⁾ *N/A	0.006	¹³⁾ *0.007	0.003	¹⁹⁾ 0.004
03C	0.0010	0.0020	⁶⁾ *0.600	$^{10}*0.011$	0.004	0.022	0.107
04C	0.0010	0.0010	⁷⁾ *0.890	$^{11)*}0.008$	¹⁵⁾⁾ *0.006	0.001	0.150
06C	0.0010	$^{1)*}0.0310$	⁸⁾ *0.890	$^{12)}*0.0007$	16)*0.001	0.006	*0.103
AVER	0.0020	0.0070	0.470	0.005	0.005	0.009	0.054
LESS			02B			· · ·	
			02C				

*See Section 2.2 regarding figures preceded by an asterisk.

Figures representing error rate (in per cent) preceded by a number 1), 2), etc., are related to legend below.

1),6),11),13)	Average 2 weeks (18,19 / 24,26 / 29,30 / 31,32)
4),5),7),8)	Average 1 week (26,24)
2),3),9),10),12)	Average 3 weeks (23,24,26 / 27,29,30 / 28-30)
14),15),16)	Average 3 weeks (31,32,35 / 31,34,35)
17)	Average 2 weeks (38,39)
18),19)	Average 5 months

Table 2.2.1 Communications performance. The numbers represent error rates in per cent based on total transmitted frames/week (1 April - 30 September 1990).

2.3 Event detection operation

In Table 2.3.1 some monthly statistics of the Detection and Event Processor operation are given. The table lists the total number of detections (DPX) triggered by the on-line detector, the total number of detections processed by the automatic event processor (EPX) and the total number of events accepted after analyst review (teleseismic phases, core phases and total).

	Total	Total	Accept	ted events		
	DPX	\mathbf{EPX}	P-phases	Core phases	Sum	Daily
Apr 90	10350	1282	300	70	370	12.3
May 90	7100	1209	348	87	435	14.0
Jun 90	7700	1326	284	70	354	11.8
Jul 90	8100	1401	482	69	551	17.8
Aug 90	8025	1203	287	79	366	11.8
Sep 90	8475	1007	233	50	283	9.4
	,		1934	425	2359	12.9

Table 2.3.1. Detection and Event Processor statistics, 1 April – 30 September 1990.

B. Paulsen

3 Operation of Regional Arrays

3.1 Recording of NORESS data at NDPC, Kjeller

Table 3.1.1 lists the main outage times and reasons, and as can be seen the main reasons for the outages are hardware failure at the HUB and line failure.

The average recording time was 92.9% as compared to 96.9% for the previous period.

Da	ate	Time	Cause
. 3	Apr	0216-0401	Power failure HUB
3	Apr	0640-0808	Power failure HUB
3	Apr	0829-1210	Power failure HUB
3	Apr	2041-2155	Power failure HUB
3	Apr	2159-	Power failure HUB
4	Apr	-1107	Power failure HUB
6	Apr	2338-	Software failure
7	Apr	-1415	Software failure
7	Apr	1742-1752	Transmission line failure
10	Apr	0511-0609	Transmission line failure
10	Apr	1200-2008	Hardware failure HUB
21	Apr	0014-0029	Transmission line failure
26	Apr	1937-1959	Transmission line maintenance
2	May	1931-	Hardware failure HUB
8	May	-1014	Hardware failure HUB
14	May	0734-	Hardware failure HUB
15	May	-0921	Hardware failure HUB
29	May	0039-0537	Transmission line failure
29	May	0555-0604	Transmission line failure
31	May	1423-1918	Power failure HUB
5	Jun	0523-1510	Software work
6	Jun	1256-1336	Transmission line failure
11	Jun	0600-0643	Transmission line failure
11	Jun	1106-1339	Transmission line failure
12	Jun	2207-2304	Power failure HUB
14	Jun	1050-1107	Hardware failure NDPC
19	Jun	2207-2319	Power break HUB
28	Jun	0859-1506	Power break HUB
28	Jun	1728-1753	Power break HUB

4	Jul	0727-	Hardware failure NDPC
5	Jul	-1718	Hardware failure NDPC
7	Jul	1102-1108	Transmission line failure
25	Jul	0830-0943	Power break NDPC
27	Jul	0004-0057	Hardware failure NDPC
27	Jul	0949-1158	Hardware failure NDPC
1	Aug	1150-1223	Hardware maintenance HUB
8	Aug	1542-1608	Hardware failure NDPC
17	Aug	1211-1235	Transmission line test
17	Aug	1259-1334	Transmission line test
21	Aug	0829-0902	Transmission line test
28	Aug	0156-0302	Power break NDPC
28	Aug	0823-1031	Power break NDPC
3	Sep	0844-0915	Power break NDPC
3	Sep	0952-1010	Power break NDPC
3	Sep	1023-1027	Power break NDPC
13	Sep	1101-1204	Transmission line test
17	Sep	1213-1234	Transmission line test
26	Sep	1239-1340	Hardware work HUB
30	Sep	0100-0200	Software failure

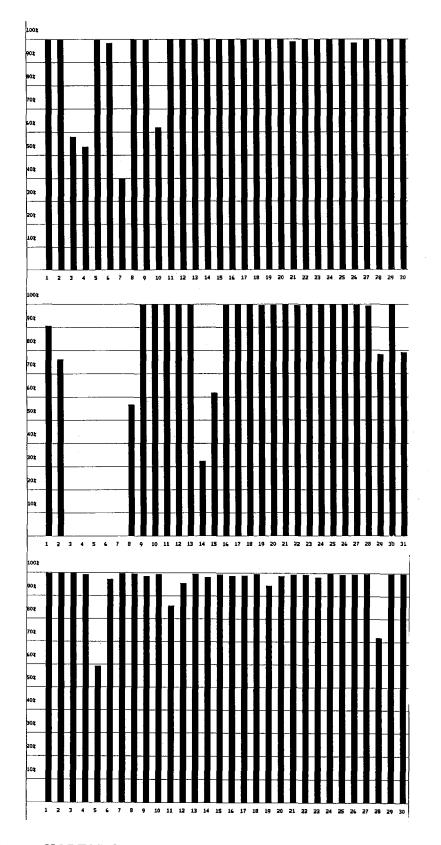
Table 3.1.1. Interruptions in recording of NORESS data at NDPC, 1 April - 30 September 1990.

Monthly uptimes for the NORESS on-line data recording task, taking into account all factors (field installations, transmissions line, data center operation) affecting this task were as follows:

April	:	93.6%
\mathbf{May}	:	76.5%
June	:	96.3%
July	:	93.6%
August	:	98.5%
September	:	98.9%

Fig. 3.1.1 shows the uptime for the data recording task, or equivalently, the availability of NORESS data in our tape archive, on a day-by-day basis, for the reporting period.

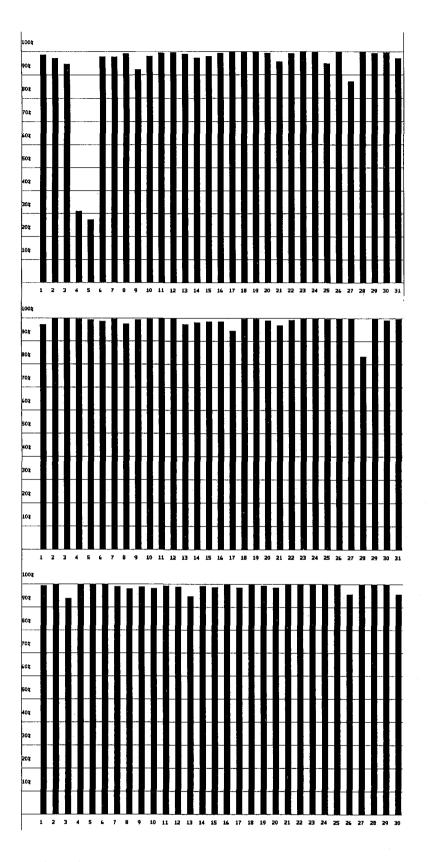
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Fig. 3.1.1. NORESS data recording uptime for April (top), May (middle) and June (bottom) 1990.



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Fig. 3.1.1. (cont.) NORESS data recording uptime for July (top), August (middle) and September (bottom) 1990.

3.2 Recording of ARCESS data at NDPC, Kjeller

The main reasons causing most of the ARCESS outage in the period are: Hardware failure at NDPC or HUB, power failure at HUB and work by the power company to reinforce the line from which power is supplied for ARCESS. Outage intervals are listed in Table 3.2.1.

The average recording time was 95.6% as compared to 95.3% for the previous period.

Date		Time	Cause		
	Apr	2058-	Power break HUB		
	Apr		Power break HUB		
	-	1322-1336	Power break HUB		
25	Apr	2100-	Power break HUB		
26	Apr	-0408	Power break HUB		
26	Apr	2110-0648	Power break HUB		
9	May	1124-1348	Software maintenance		
10	May	1426-	Hardware failure NDPC		
11	May	-0451	Hardware failure NDPC		
11	May	0641-0819	Hardware failure NDPC		
13	May	2102-	Work on powerline HUB		
14	May	-0605	Work on powerline HUB		
14	May	2101-	Work on powerline HUB		
15	May	-0527	Work on powerline HUB		
15	May	2100-	Work on powerline HUB		
16	May	-0535	Work on powerline HUB		
20	May	2102-	Work on powerline HUB		
21	May	-0324	Work on powerline HUB		
21	May	2102-	Work on powerline HUB		
22	May	-0608	Work on powerline HUB		
22	May	2058-	Work on powerline HUB		
23	May	-0451	Work on powerline HUB		
25	May	2219-2319	Hardware failure NDPC		
26	May	1315-1348	Hardware failure NDPC		
6	Jun	1747-1916	Transmission line failure		
7	Jun	1540-1724	Transmission line failure		
8	Jun	1019-1052	Hardware failure NDPC		
10	Jun	1149-1210	Hardware failure NDPC		
1	Jul	0828-0912	Software failure		
3	Jul	1437-	Transmission line failure		

4	Jul	-1011	Transmission line failure
5	Jul	1058-1115	Software failure
5	Jul	1502-1553	Software failure
7	Jul	0850-0913	Software failure
7	Jul	1434-1447	Hardware failure NDPC
8	Jul	0902-0925	Hardware failure NDPC
9	Jul	2112-2125	Software failure
14	Jul	0504-0620	Software failure
14	Jul	1730-1738	Software failure
21	Jul	2134-	Software failure
22	Jul	-0809	Software failure
23	Jul	1156-	Hardware failure HUB
24	Jul	-1854	Hardware failure HUB
25	Jul	0757-0839	Power break NDPC
3	Aug	0705-0814	Software failure
4	Aug	0942-0952	Software failure
22	Aug	0437-0522	Software failure
23	Aug	0531-0556	Software failure
23	Aug	1832-1849	Software failure
28	Aug	0114-0305	Power break NDPC
28	Aug	0548-0715	Power break NDPC
28	Aug	0823-1031	Power break NDPC
3	Sep	0844-0915	Power break NDPC
3	Sep	0952-1010	Power break NDPC
3	Sep	1023-1027	Power break NDPC
13	Sep	2238-	Hardware failure NDPC
14	Sep	-0529	Hardware failure NDPC
20	Sep	1329-1339	Work on power NDPC
20	Sep	1632-1749	Power break HUB
25	Sep	1529-	Hardware failure NDPC
26	Sep	-0539	Hardware failure NDPC

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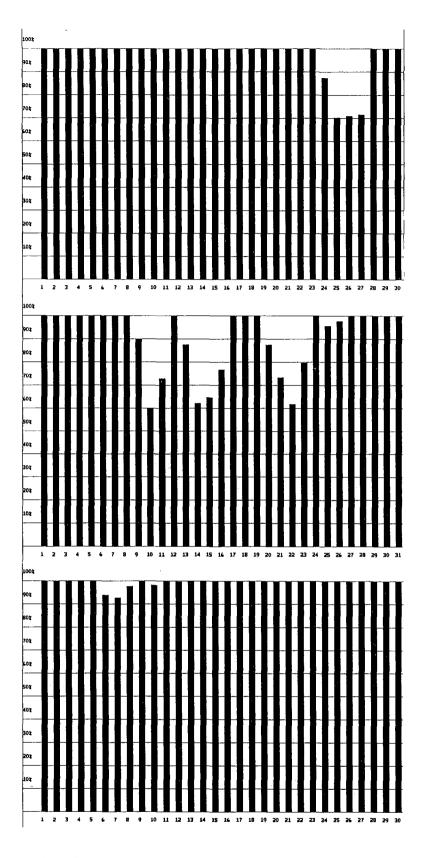
Table 3.2.1. The main interruptions in recording of ARCESS data at NDPC, 1 April - 30 September 1990.

Monthly uptimes for the ARCESS on-line data recording task, taking into account all factors (field installations, transmissions line, data center operation) affecting this task were as follows:

April	:	96.7%
\mathbf{May}	:	90.7%
June	:	99.4%
July	:	91.1%
August	:	98.9%
September	:	96.7%

Fig. 3.2.1 shows the uptime for the data recording task, or equivalently, the availability of ARCESS data in our tape archive, on a day-by-day basis, for the reporting period.

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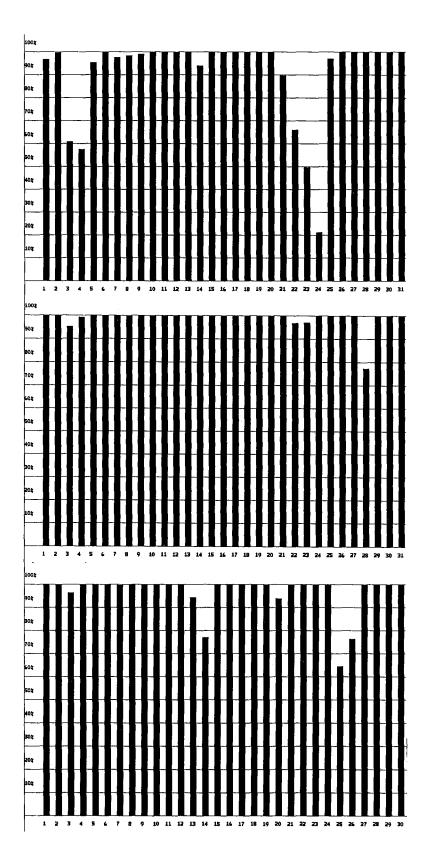
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Fig. 3.2.1. ARCESS data recording uptime for April (top), May (middle) and June (bottom) 1990.



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Fig. 3.2.1. (cont.) ARCESS data recording uptime for July (top), August (middle) and September (bottom) 1990.

3.3 Recording of FINESA data at NDPC, Kjeller

The average recording time was 39.0% as compared to 98.5% for the previous period. The main reason for the low uptime of the FINESA array was a thunderstorm on May 22 that put the field computer out of operation until August 26 except for a few hours on June 19.

Date	Time	Cause
2 May	0625-	Hardware/software problems NDPC
8 May	-1925	Hardware/software problems NDPC
15 May	0044-0119	Transmission line failure
15 May	1653-	Transmission line failure
16 May	-1103	Transmission line failure
22 May	0926-	Hardware failure HUB
19 Jun	-0752	Hardware failure HUB
19 Jun	1231-	Hardware failure HUB
26 Aug	-0830	Hardware failure HUB
26 Aug	2328-	Hardware failure HUB
29 Aug	-0955	Hardware failure HUB
29 Aug	1002-1009	Hardware failure HUB
31 Aug	1132-1956	Hardware failure HUB
6 Sep	0940-	Transmission line failure
12 Sep	-0805	Transmission line failure
13 Sep	2314-2332	Transmission line failure
14 Sep	0030-0054	Transmission line failure
18 Sep	0515-0520	Transmission line failure
20 Sep	1328-1400	Maintenance NDPC
20 Sep	1718-1737	Maintenance NDPC
26 Sep	0958-1019	Transmission line failure
26 Sep	1037-1154	Transmission line failure
27 Sep	0743-1302	Transmission line failure

Table 3.3.1 The main interruptions in recording of FINESA data at NDPC, 1 April - 30 September 1990.

Monthly uptimes for the FINESA on-line data recording task, taking into account all factors (field installations, transmissions line, data center operation) affecting this task were as follows:

April	:	100.0%
May	:	45.0%
June	:	0.6%
July	:	0.0%
August	:	9.2%
September	:	79.0%

Fig. 3.3.1 shows the uptime for the data recording task, or equivalently, the availability of FINESA data in our tape archive, on a day-by-day basis, for the reporting period.

J. Torstveit

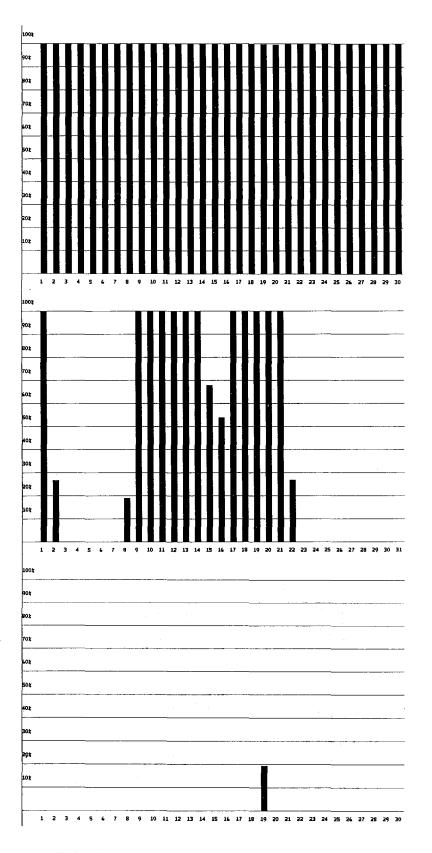


Fig. 3.3.1. FINESA data recording uptime for April (top), May (middle) and June (bottom) 1990.

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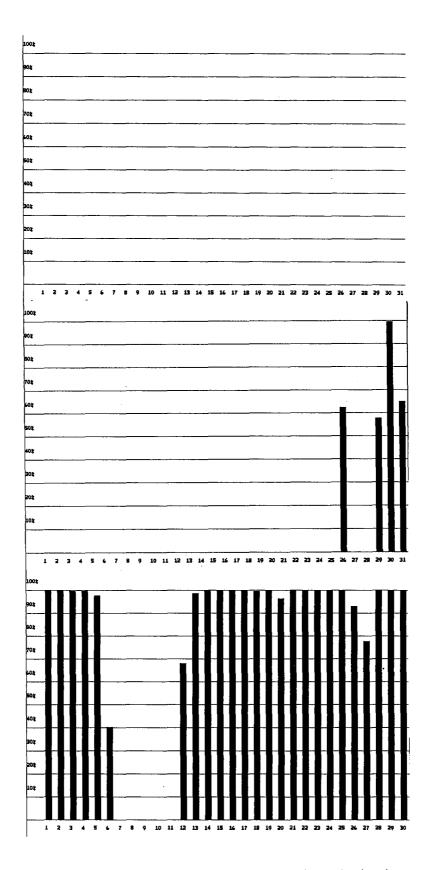


Fig. 3.3.1. (cont.) FINESA data recording uptime for July (top), August (middle) and September (bottom) 1990.

3.4 Event detection operation

NORESS detections

The number of detections (phases) reported during day 091, 1990, through day 273, 1990, was 43734, giving an average of 239 detections per processed day (183 days processed).

Table 3.4.1 shows daily and hourly distribution of detections for NORESS.

Events automatically located by NORESS

During days 091, 1990, through 273, 1990, 2275 local and regional events were located by NORESS, based on automatic association of P- and S-type arrivals. This gives an average 12.4 events per processed day (183 days processed). 60 % of these events are within 300 km, and 86 % of these events are within 1000 km.

ARCESS detections

The number of detections (phases) reported during day 091, 1990, through day 273, 1990, was 84203, giving an average of 460 detections per processed day (183 days processed).

Table 3.4.2 shows daily and hourly distribution of detections for ARCESS.

Events automatically located by ARCESS

During days 091, 1990, through 273, 1990, 4307 local and regional events were located by ARCESS, based on automatic association of P- and S-type arrivals. This gives an average 23.5 events per processed day (178 days processed). 49 % of these events are within 300 km, and 84 % of these events are within 1000 km.

FINESA detections

The number of detections (phases) reported during day 091, 1990, through day 273, 1990, was 28235, giving an average of 392 detections per processed day (72 days processed).

Table 3.4.3 shows daily and hourly distribution of detections for FINESA.

Events automatically located by FINESA

During days 091, 1990, through 273, 1990, 1385 local and regional events were located by FINESA, based on automatic association of P- and S-type arrivals. This gives an average 19.2 events per processed day (72 days processed). 68 % of these events are within 300 km, and 87 % of these events are within 1000 km.

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Day 00 01 02 03 04 05 06 07 08 09 10 11 12 13 14 15 16 17 18 19 20 21 22 23 Sum Date

249 May 27 Sunday 0 13 11 9 3 2 16 3 15 6 7 15 16 10 29 11 16 24 6 11 9 11 265 May 28 Monday 5 12 4 10 0 10 14 17 13 19 10 16 13 17 16 17 18 19 6 2 12 2 10 11 9 9 19 22 15 9 2 6 20 13 6 14 2 179 May 29 Tuesday 15 19 15 14 20 24 35 15 10 12 10 12 6 8 1 6 309 May 30 Wednesday 3 12 $21 \ 16$ 9 21 12 8 10 21 15 12 7 0 0 0 0 16 14 213 May 31 Thursday $10 \ 11$ 7 16 4 13 29 11 9 10 12 2 11 0 19 15 15 9 43 10 12 15 8 14 298 Jun 01 Friday 19 16 19 27 23 33 17 23 29 20 24 7 10 14 12 7 12 11 361 Jun 02 Saturday 12 7 13 3 8 14 6 5 27 15 14 4 3 12 174 Jun 03 Sunday 7 12 2 5 10 14 17 23 23 12 4 10 211 Jun 04 Monday 1 0 0 0 0 0 0 0 0 19 18 22 16 26 20 32 19 27 224 Jun 05 Tuesday 7 1 10 б $22 \ 22 \ 26 \ 29 \ 25 \quad 7 \ 13 \ 20 \ 19 \ 17 \ 15 \ 27 \ 16 \ 11 \ 31 \ 31 \ 15 \ 20 \ 32 \ 18 \ 20 \ 24 \ 20 \ 34$ 514 Jun 06 Wednesday 30 33 31 33 24 14 12 13 20 24 31 22 25 24 25 21 16 13 15 14 26 16 30 29 541 Jun 07 Thursday 29 15 16 13 9 11 7 6 22 16 15 15 8 19 7 21 19 21 14 19 24 13 19 24 382 Jun 08 Friday 20 20 26 27 33 21 23 21 17 45 61 50 20 24 14 45 20 35 36 31 37 38 24 23 711 Jun 09 Saturday 29 38 32 28 19 22 17 8 11 6 7 12 13 11 14 13 21 18 14 18 13 6 7 12 389 Jun 10 Sunday 3 6 0 6 6 11 8 1 0 4 14 6 17 8 13 7 19 2 17 197 Jun 11 Monday $15 \ 12 \ 12$ 8 17 14 19 1 11 6 11 1 13 17 22 11 15 16 10 22 31 28 8 26 5 1 19 332 Jun 12 Tuesday 9 8 11 14 14 11 12 15 18 11 13 11 12 5 11 13 8 9 264 Jun 13 Wednesday 9 10 18 8 3 11 5 22 10 9 14 18 19 21 14 13 4 7 14 22 15 2 12 14 2 16 10 3 3 277 Jun 14 Thursday 1 11 5 11 7 15 14 15 19 19 13 6 9 9 6 16 12 2 3 223 Jun 15 Friday 3 10 26 4 3 15 5 5 14 6 15 2 0 11 4 4 1 5 1 3 167 Jun 16 Saturday 4 3 0 15 4 5 3 4 13 8 11 13 12 1 13 20 2 13 167 Jun 17 Sunday 3 12 6 8 12 5 5 17 8 10 10 13 19 15 9 8 25 1 $2 \ 11$ 2 30 247 Jun 18 Monday 9 11 4 38 13 24 12 8 18 11 10 2 22 15 8 - 7 247 Jun 19 Tuesday 29 16 18 6 14 17 18 18 14 23 17 8 25 294 Jun 20 Wednesday 6 11 13 4 20 20 21 18 26 15 24 30 18 17 20 13 349 Jun 21 Thursday 0 8 17 6 12 15 20 12 10 7 18 16 2 1 15 229 Jun 22 Friday 14 10 15 13 18 9 17 13 10 9 15 6 10 13 6 14 4 23 16 14 215 Jun 23 Saturday 4 14 1 2 10 13 5 222 Jun 24 Sunday 1 16 15 3 14 13 12 20 19 22 11 5 9 18 10 5 15 16 14 9 193 Jun 25 Monday 4 9 15 7 14 6 10 10 9 15 28 13 14 9 22 10 18 5 14 32 28 10 16 12 11 330 Jun 26 Tuesday 14 8 8 11 17 26 20 8 16 22 12 6 8 24 8 16 7 6 6 10 289 Jun 27 Wednesday 13 13 13 0 0 0 0 0 0 4 11 11 16 9 21 5 2 13 176 Jun 28 Thursday 12 11 19 1 5 6 16 7 8 11 22 26 9 13 15 24 15 10 6 9 16 5 9 13 7 1 9 249 Jun 29 Friday $2 \ 11$ 2 31 8 11 17 10 12 13 28 20 13 15 23 25 10 4 269 Jun 30 Saturday 2 13 0 1 3 17 8 7 20 17 6 10 8 15 6 19 16 14 12 7 268 Jul 01 Sunday 8 14 14 12 11 7 5 12 10 15 4 13 9 10 20 1 16 6 4 14 206 Jul 02 Monday 308 Jul 03 Tuesday 5 11 7 12 17 5 19 19 16 8 18 16 15 19 21 21 20 29 б 0 0 145 Jul 04 Wednesday 0 0 0 0 27 21 26 20 15 0 0 0 0 9 20 13 15 4 6 10 77 Jul 05 Thursday $1 \ 11 \ 1 \ 18$ 6 14 14 10 4 18 15 10 10 10 4 4 10 216 Jul 06 Friday 8 11 0 14 4 5 0 14 15 20 19 36 22 18 26 28 26 29 322 Jul 07 Saturday 19 34 27 32 23 26 25 13 22 19 14 13 15 17 15 11 21 3 6 8 439 Jul 08 Sunday 5 12 1 14 13 7 12 19 10 19 13 23 11 12 9 2 207 Jul 09 Monday 7 13 16 24 13 12 7 10 15 4 5 11 14 13 10 208 Jul 10 Tuesday 2 13 15 8 10 14 10 20 8 10 11 11 12 4 11 192 Jul 11 Wednesday 84 20 14 47 34 20 11 33 17 5 9 7 9 23 14 380 Jul 12 Thursday 4 10 2 12 5 13 17 14 12 17 6 12 16 13 10 15 12 231 Jul 13 Friday 19 44 17 46 34 12 17 28 14 11 10 4 6 13 340 Jul 14 Saturday 2 2 2 9 7 3 0 4 5 9 17 24 13 2 14 11 7 11 162 Jul 15 Sunday 8 3 47 65 36 41 21 28 54 22 18 15 25 20 18 18 14 13 16 511 Jul 16 Monday 6 13 0 0 5 16 10 19 19 12 11 25 28 6 0 0 0 0 0 0 0 201 Jul 17 Tuesday 6 27 2 17 486 Jul 18 Wednesday 0 0 0 2 11 40 36 64 25 23 33 79 30 21 14 22 12 51 4 6 22 30 2 14 17 10 5 8 36 15 15 26 20 10 11 17 7 6 16 2 3 10 309 Jul 19 Thursday 4 24 4 12 38 6 8 7 17 13 12 10 6 10 10 32 31 30 13 7 5 3 25 329 Jul 20 Friday 3 20 8 14 7 12 12 6 10 12 6 4 13 11 7 8 6 14 9 14 0 2 4 204 Jul 21 Saturday

Table 3.4.1. (Page 2 of 4)

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254 255 256	8 4 13	31 19 76	9 10 13 3 9 7	5 9 12 13 13 22		2 10 3 26 5 0	23	$ \begin{array}{cccc} 16 & 16 \\ 21 & 12 \\ 16 & 7 \end{array} $	7	8	23 8 18	1 9 8	8 14 7	13 5 14	3 4 2	4 5 5	8 11 5		Sep	12	Tuesday Wednesday Thursday
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Table 3.4.1. (Page 3 of 4)

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Table 3.4.1. Daily and hourly distribution of NORESS detections. For each day is shown number of detections within each hour of the day, and number of detections for that day. The end statistics give total number of detections distributed for each hour and the total sum of detections during the period. The averages show number of processed days, hourly distribution and average per processed day. (Page 4 of 4)

Day 00 01 02 03 04 05 06 07 08 09 10 11 12 13 14 15 16 17 18 19 20 21 22 23 Sum Date

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Table 3.4.2. (Page 3 of 4)

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Table 3.4.2. Daily and hourly distribution of ARCESS detections. For each day is shown number of detections within each hour of the day, and number of detections for that day. The end statistics give total number of detections distributed for each hour and the total sum of detections during the period. The averages show number of processed days, hourly distribution and average per processed day. (Page 4 of 4)

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238 239 240 241 242 243 243 244 245	0 0 13 20 4 3	0 0 0 9 29 6 5	0 0 0 18 9 7 0	0 0 0 6 5 2 3	0 0 16 12 3 6	0 0 0 14 15 1 4	0 0 0 13 14 1 7	0 0 23 18 5 6	0 0 25 26 2 5	0 0 20 24 7	0 0 27 21 20 8 6	0 0 23 32 29 3 18	0 0 17 17 0 6 9	0 0 18 24 0 8 7	0 0 15 23 0 4 6	0 0 6 16 8 3	0 0 24 17 0 5 5	0 0 8 20 0 5 12	0 0 15 13 0 7 9	0 0 8 11 7 3	0 0 3 11 7 8 13	0 0 8 6 3 5 4	0 0 4 8 3 5 6	0 0 13 9 12 0 3	0 2 0 2 189 2 385 2 246 2 110 2 150 2	Aug Aug Aug Aug Aug Sep Sep	27 28 29 30 31 01 02	Sunday Monday Tuesday Wednesday Thursday Friday Saturday Sunday
246 247 248 250 251 252 253 253 254	7 8 5 2 0 0 0 0 0	7 10 6 7 0 0 0 0 0 0	8 5 7 9 0 0 0 0 0	3 8 4 0 0 0 0 0	3 2 1 5 0 0 0 0 0	3 2 5 6 0 0 0 0 0	0 2 8 4 0 0 0 0 0	6 4 11 10 0 0 0 0 0	10 16 15 18 0 0 0 0	5 12 23 13 0 0 0 0 0	18 15 15 0 0 0 0 0 0	23 26 21 0 0 0 0 0 0	9 15 17 0 0 0 0 0 0	16 11 13 0 0 0 0 0 0	7 7 14 0 0 0 0 0 0	3 12 3 0 0 0 0 0 0 0	3 2 1 0 0 0 0 0 0 0		10 4 2 0 0 0 0 0 0 0	3 4 0 0 0 0 0 0 0	12 4 1 0 0 0 0 0 0 0	8 10 5 0 0 0 0 0 0 0	8 4 5 0 0 0 0 0 0	12 5 9 0 0 0 0 0 0 0	193 209 78 0 0 0	Sep Sep Sep Sep Sep Sep Sep	04 05 06 07 08 09 10	Monday Tuesday Wednesday Thursday Friday Saturday Sunday Monday Tuesday
254 255 256 257 258	0 9 11 4	0 7 8 4	0 12 8 7	0 4 13 10	0 8 10 9	0 5 10 11	0 3 14 13	13 7 20	13 22 27 13	16 15 26	27 22 28	25 29 25 21	14 24 4	16 24 9 26	11 10 6 28	8 6 3 2	5 4 6	8 8 13 5	4 7 4 2	5 12 2 0	8 3 7 5	9 5 3 4	13 11 2 3	5 4 4 8	200 s 261 s 263 s	Sep Sep Sep	12 13 14	Wednesday Thursday Friday Saturday

Table 3.4.3. (Page 3 of 4)

Day 00 01 02 03 04 05 06 07 08 09 10 11 12 13 14 15 16 17 18 19 20 21 22 23 Sum Date

0 6 6 2 4 6 7 3 4 10 11 11 10 259 3 0 2 5 4 16 7 11 5 138 Sep 16 Sunday 7 13 7 1 9 3 17 35 37 26 40 28 19 24 37 7 7 5 9 7 327 Sep 17 Monday 260 6 6 4 5 21 20 26 24 24 16 37 31 19 19 6 11 8 261 10 11 10 9 б 8 5 б 1 9 342 Sep 18 Tuesday 7 5 262 5 - 9 5 5 9 14 20 13 17 20 11 14 54 5 - 6 4 6 1 6 4 5 200 Sep 19 Wednesday 6 10 11 15 24 26 40 21 26 26 8 8 3 3 1 5 11 10 11 4 11 306 Sep 20 Thursday 263 6 12 8 6 4 7 6 5 26 20 19 24 12 17 7 2 5 3 225 Sep 21 Friday 264 12 12 8 5 6 10 2 52 5 4 17 13 8 28 22 29 35 41 26 31 34 32 33 40 50 52 29 36 55 42 45 58 265 765 Sep 22 Saturday 266 53 57 36 23 21 36 62 56 51 57 37 28 18 19 7 9 6 4 17 13 8 15 21 14 668 Sep 23 Sunday 10 14 12 1 4 0 6 10 10 13 14 25 13 11 16 14 8 8 8 11 10 6 267 47 235 Sep 24 Monday 268 13 7 7 13 53 5 12 16 9 21 15 28 18 6 4 2 9 6 10 6 8 7 7 237 Sep 25 Tuesday 2 3 7 12 13 3 0 19 15 10 10 6 7 3 1 б 5 161 Sep 26 Wednesday 269 7 10 4 45 3 б 270 3 11 3 2 4 2 4 2 0 0 0 0 0 16 6 11 5 3 5 1 6 13 6 8 111 Sep 27 Thursday 6 14 10 6 7 4 5 10 17 17 23 22 16 3 4 7 5 б 5 4 12 2 41 210 Sep 28 Friday 271 4 2 2 3 2 11 19 12 8 10 18 16 8 13 4 13 7 272 4 3 1 1 7 3 1 172 Sep 29 Saturday 5 3 4 9 0 5 7 11 13 5 9 8 3 3 4 4 5 2 6 12 14 11 7 12 162 Sep 30 Sunday 273 FIN 00 01 02 03 04 05 06 07 08 09 10 11 12 13 14 15 16 17 18 19 20 21 22 23 615 1042 1548 2581 1999 1347 883 Sum 759 573 813 759 753 728 1413 1888 2194 1870 2159 807 28235 Total sum 670 636 559 843 796 9 11 9 8 8 9 10 14 20 22 26 36 30 28 26 19 30 12 12 11 11 11 11 10 392 Total average 72 8 6 7 9 14 20 22 29 43 38 34 32 21 38 12 11 12 11 11 12 10 429 Average workdays 48 10 10 9 12 9 9 12 11 13 15 18 21 21 22 15 14 14 13 14 13 12 11 11 9 11 11 319 Average weekends 24

Table 3.4.3. Daily and hourly distribution of FINESA detections. For each day is shown number of detections within each hour of the day, and number of detections for that day. The end statistics give total number of detections distributed for each hour and the total sum of detections during the period. The averages show number of processed days, hourly distribution and average per processed day. (Page 4 of 4)

3.5 IMS operation

The Intelligent Monitoring System (IMS) was installed at NORSAR in December 1989 and has been operated experimentally since 1 January 1990 for automatic processing of multiple-array data. The current version of IMS processes data from the two-array network consisting of NORESS and ARCESS. Future upgrades of IMS will allow data from additional arrays and single stations to be incorporated.

In general, our routine operation of the IMS during the reporting period has progressed well, and the system has proved to be very powerful and flexible. The well-developed automatic processing combined with very versatile interactive tools has kept the analyst workload at a low level, and in fact only one analyst has been required to handle the regular processing at any time.

Since the IMS is still in an initial stage, there have naturally been some problems of a technical nature, but these have diminished considerably as the system has matured. At the end of the reporting period, the IMS system is running very smoothly.

Table 3.5.1 presents an overview of IMS event processor downtimes. Table 3.5.2 gives a summary of phase detections and processed regional events by IMS. From top to bottom, the table gives the total number of detections by the IMS, the detections that are associated with regional events declared by the IMS, the number of detections that are not associated with such events, the number of regional events declared by the IMS, the number of such events declared by the analyst, the number of events accepted by the analyst, the number of events accepted by the analyst without any changes, and finally the number of events accepted after some sort of modification by the analyst. This last category is divided into three classes: Events where phases (not detected by the IMS) have been added by the analyst, events for which the phase assignments by the IMS have been changed or one or more phase detections have been removed, and events for which the changes by the analyst have amounted to retiming the phases only.

From initial review of the IMS bulletin, it is clear that the final output is of very high quality from a seismological point of view. More detailed evaluation will be conducted at a later stage.

B.Kr. Hokland U. Baadshaug S. Mykkeltveit

1	.990	May	29	14:47:01.000	-	1990	May	30	10:06:07.000
1	990	May	30	13:13:30.000		1990	May	31	18:30:50.379
1	990	Jun	8	14:20:32.713	-	1990	Jun	9	08:00:00.000
1	.990	Jun	9	12:55:30.000	-	1990	Jun	9	22:30:51.000
1	1990	Jun	10	11:22:22.752	-	1990	Jun	11	10:00:00.000
1	1990	Jun	15	13:23:21.700	-	1990	Jun	16	00:00:00.000
1	990	Jun	16	13:24:57.500	-	1990	Jun	19	00:00:00.000
1	1990	Jun	22	20:13:36.000	-	1990	Jun	26	00:00:00.000
1	1990	Jun	26	03:34:17.000	-	1990	Jun	26	18:27:20.000
1	1990	Jun	30	10:20:53.800	-	1990	Jul	1	00:00:00.000
1	1990	Jul	6	07:45:52.000	-	1990	Jul	7	00:00:00.000
1	1990	Jul	9	17:56:50.500	-	1990	Jul	10	00:00:00.000
1	1990	Jul	10	23:29:23.700	-	1990	Jul	12	00:00:00.000
1	1990	Jul	13	13:26:07.600	-	1990	Jul	15	00:00:00.000
1	1990	Jul	16	16:15:52.800	-	1990	Jul	17	00:00:00.000
1	1990	Jul	17	09:17:33.300	-	1990	Jul	19	00:00:00.000
1	1990	Jul	19	21:39:56.200	-	1990	Jul	22	10:56:47.400
1	1990	Jul	22	20:27:00.000	-	1990	Jul	24	00:24:57.933
1	1990	Jul	24	09:55:22.500	-	1990	Jul	24	23:35:08.241
1	1990	Aug	5	05:26:02.840	-	1990	Aug	6	05:18:15.167
1	1990	Aug	13	20:15:28.400	-	1990	Aug	17	18:00:00.000
1	1990	Aug	18	20:38:30.200	-	1990	Aug	19	18:00:00.000
1	1990	Sep	1	05:14:22.800	-	1990	Sep	2	00:00:00.000
1	1990	Sep	10	04:43:55.100	-	1990	Sep	24	00:00:00.000
1	1990	Sep	28	09:40:09.800	-	1990	Sep	29	00:00:00.000
1	1990	Sep	30	10:29:13.300	-	1990	Sep	30	24:00:00.000

Table 3.5.1. IMS event processor (pipeline) downtimes. Logging of time intervals not processed by the event processor (pipeline) started the last week of May. The main reason for these downtimes was slow performance of the event processing, causing loss of waveform data from the disk before the events were processed.

	Apr 90	May 90	Jun 90	Jul 90	Aug 90	Sep 90	total
Phase detections	11843	13988	13178	10989	19267	15402	84667
- Associated phases	1685	2521	1863	1125	2361	1021	10576
- Unassociated phases	10158	11467	11315	9864	16906	14381	74091
Events declared	708	1002	834	493	943	278	4258
- Rejected events	183	196	237	131	218	43	1009
- Accepted events	525	806	597	361	725	235	3249
Unchanged events	85	186	293	172	290	78	1104
Modified events	440	620	304	189	435	157	2145
Phases added	46	63	23	9	30	16	187
Phases changed or removed	281	402	270	180	405	141	1679
Retiming only	113	155	11	0	0	0	279

Table 3.5.2. IMS phase detections and events summary. Statistics for "retiming only" have been compiled only up to June 4.

4 Improvements and Modifications

4.1 NORSAR

NORSAR data acquisition

No modification has been made to the NORSAR data acquisition system.

RD3 digitizers and acquisition equipment have been acquired from Nanometrics

to test recording at one subarray. There are two major tasks that need to be worked upon:

- 1. Solving the problem of getting enough DC current from the central vault to the digitizer at the seismometer.
- 2. Including SDLC communication in the Nanometrics system to get a continuous data stream from the subarray to the NORSAR data processing center. (This is currently not offered by the manufacturer.)

NORSAR detection processing

The NORSAR detection processor has been running satisfactorily on the IBM during this reporting period.

Detection statistics are given in section 2.

NORSAR event processing

There are no changes in the routine processing of NORSAR events, using the IBM system.

4.2 NORESS/ARCESS/FINESA/GERESS

Detection processing

The routine detection processing of the arrays is running satisfactorily on each of the arrays' SUN-3/280 acquisition systems. The same program is used for NORSAR/NORESS/ARCESS/ FINESA/GERESS, but with different recipes. The beam table for NORESS/ARCESS is found in NORSAR Sci. Rep. No. 1-89/90. A new beam table for FINESA is found in Table 4.2.1. This change of the beam table is related to changes in the FINESA array geometry in August. A new vertical sensor was installed at the array center (A0), and horizontal sensors were added at the existing A1 site. Test processing of GERESS data has been started, and the initial beam table is shown in Table 4.2.2.

Event processing. Phase estimation

This process does F-K and polarization analysis for each detection to determine phase velocity, azimuth and type of phase.

The processing using the EP program is now running on the IMS machines, and detections are put into the ORACLE detection data base for use by IMS.

Plot and epicenter determination

A description of single array event processing is found in NORSAR Sci. Rep. No. 2-88/89, and NORSAR Sci. Rep. No. 2-89/90.

J. Fyen

22	10100103	112 1114 011	1 11 001	Juna	1111 0011014	00111	+Baraoro
C011	99999.9	0.0	0.5 -	1.5	4.4	7	С
C021	99999.9	0.0	1.0 -	3.0	4.4	7	С
C031	99999.9	0.0	1.5 -	3.5	4.4	7	С
C032	11.0	30.0	1.5 -	3.5	4.4	7	C
C033	11.0	90.0	1.5 -	3.5	4.4	7	С
C034	11.0	150.0	1.5 -	3.5	4.4	7	С
C035	11.0	210.0	1.5 -	3.5	4.4	7	С
C036	11.0	270.0	1.5 -	3.5	4.4	7	С
C037	11.0	330.0	1.5 -	3.5	4.4	7	С
C038	15.0	80.0	1.5 -	3.5	3.9	7	С
C039	10.0	20.0		3.5	3.9	7	С
C041	99999.9	0.0				7	
C042	10.2	30.0				7	C
C043	10.2	90.0	2.0 -			7	С
C044	10.2	150.0	2.0 -		4.4	7	C
C045	10.2	210.0				7	C
C046	10.2	270.0	2.0 -		4.4	7	C
C047	10.20	330.0	2.0 -		4.4	7	С
C048	15.0	80.0				7	C
C049	10.0	20.0				7	C
C051	99999.9	0.0				13	BC
C052	8.9	30.0	2.5 -		4.4	13	BC
C053	8.9	90.0				13	BC
C054	8.9	150.0				13	BC
C055	8.9	210.0	2.5 -		4.4	13	BC
C056	8.9	270.0	2.5 -			13	BC
C057	8.9	330.0				13	BC
C058	15.0	80.0				13	BC
C061	99999.9	0.0	3.0 -		4.4	13	BC
C062	10.5	30.0				13	BC
	10.5					13	BC
C064	10.5	150.0	3.0 -		4.4	13	BC
C065 C066	10.5	210.0	3.0 -		4.4	13	BC
	10.5	270.0	3.0 -			13	BC
C067 C068	10.5 15.0	330.0 80.0	3.0 -		4.4	13	BC
C088	999999.9	0.0	3.0 - 3.5 -		3.9	13 16	BC
C071	11.1	30.0				16 16	ABC
C072	11.1	90.0	3.5 - 3.5 -		4.4 4.4	16 16	ABC ABC
0015	****	30.0	5.5 -	0.0	7.4	10	ADU

BEAM Velocity Azimuth Filter band Threshold Configuration

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C074	11.1	150.0	3.5 - 5.5	4.4	16	ABC
C075	11.1	210.0	3.5 - 5.5	4.4	16	ABC
C076	11.1	270.0	3.5 - 5.5	4.4	16	ABC
C077	11.1	330.0	3.5 - 5.5	4.4	16	ABC
C081	99999.9	0.0	4.0 - 8.0	4.4	16	ABC
C082	9.5	30.0	4.0 - 8.0	4.4	16	ABC
C083	9.5	90.0	4.0 - 8.0	4.4	16	ABC
C084	9.5	150.0	4.0 - 8.0	4.4	16	ABC
C085	9.5	210.0	4.0 - 8.0	4.4	16	ABC
C086	9.5	270.0	4.0 - 8.0	4.4	16	ABC
C087	9.5	330.0	4.0 - 8.0	4.4	16	ABC
C091	99999.9	0.0	5.0 - 10.0	4.9	16	ABC
C092	10.5	30.0	5.0 - 10.0	4.9	16	ABC
C093	10.5	90.0	5.0 - 10.0	4.9	16	ABC
C094	10.5	150.0	5.0 - 10.0	4.9	16	ABC
C095	10.5	210.0	5.0 - 10.0	4.9	16	ABC
C096	10.5	270.0	5.0 - 10.0	4.9	16	ABC
C097	10.5	330.0	5.0 - 10.0	4.9	16	ABC
C101	99999.9	0.0	8.0 - 16.0	4.9	10	AB
C102	9.9	30.0	8.0 - 16.0	4.9	10	AB
C103	9.9	90.0	8.0 - 16.0	4.9	10	AB
C104	9.9	150.0	8.0 - 16.0	4.9	10	AB
C105	9.9	210.0	8.0 - 16.0	4.9	10	AB
C106	9.9	270.0	8.0 - 16.0	4.9	10	AB
C107	9.9	330.0	8.0 - 16.0	4.9	10	AB
CIO1	99999.9	0.0	0.5 - 1.5	2.9	7	С
CI02	99999.9	0.0	1.0 - 2.0	2.9	7	С
CIO3	99999.9	0.0	1.5 - 2.5	2.9	7	С
CI04	99999.9	0.0	2.0 - 4.0	2.5	7	С
CI05	99999.9	0.0	3.5 ~ 5.5	2.5	7	С
CI06	99999.9	0.0	5.0 - 10.0	2.7	7	С

Table 4.2.1. FINESA beam table. Valid from 1990-237: (25 august 1990), when A0 was included. The table shows name of beam, velocity (km/sec), azimuth (degrees), filter band (Hz), STA/LTA threshold, and configuration. The configuration is described with number of sensors and A, B or C-rings. The sensor at A0 is included in all configurations. CI01 – CI06 are incoherent beams.

BEAM	Velocity	Azimuth	Filter	band	Threshold	Config	uration
G011	99999.9	0.0	0.5 -	1.5	4.5	10	D
G021	99999.9	0.0	1.0 -	3.0	4.5	17	CD
G031	99999.9	0.0	1.5 -	3.5	4.5	17	CD
G032	11.0	30.0	1.5 -	3.5	4.5	17	CD
G033	11.0	90.0	1.5 -	3.5	4.5	17	CD
G034	11.0	150.0	1.5 -	3.5	4.5	17	CD
G035	11.0	210.0	1.5 -	3.5	4.5	17	CD
G036	11.0	270.0	1.5 -	3.5	4.5	17	CD
G037	11.0	330.0	1.5 -	3.5	4.5	17	CD
G038	15.8	80.0	1.5 -	3.5	4.5	17	CD
G039	10.0	30.0	1.5 -	3.5	4.5	17	CD
G041	99999.9	0.0	2.0 -	4.0	4.5	17	CD
G042	10.2	30.0	2.0 -	4.0	4.5	17	CD
G043	10.2	90.0	2.0 -	4.0	4.5	17	CD
G044	10.2	150.0	2.0 -	4.0	4.5	17	CD
G045	10.2	210.0	2.0 -	4.0	4.5	17	CD
G046	10.2	270.0	2.0 -	4.0	4.5	17	CD
G047	10.2	330.0	2.0 -	4.0	4.5	17	CD
G048	15.8	80.0	2.0 -	4.0	4.5	17	CD
G049	10.0	30.0	2.0 -		4.5	17	CD
G051	99999.9	0.0	2.5 -	4.5	4.5	22	BCD
G052	8.9	30.0	2.5 -	4.5	4.5	22	BCD
G053	8.9	90.0	2.5 -	4.5	4.5	22	BCD
G054	8.9	150.0	2.5 -	4.5	4.5	22	BCD
G055	8.9	210.0	2.5 -	4.5	4.5	22	BCD
G056	8.9	270.0	2.5 -	4.5	4.5	22	BCD
G057	8.9	330.0	2.5 -	4.5	4.5	22	BCD
G058	15.8	80.0	2.5 -	4.5	4.5	22	BCD
G059	10.0	30.0	2.5 -		4.5	22	BCD
G061	99999.9	0.0	3.0 -		4.5	22	BCD
G062	10.5	30.0	3.0 -	5.0	4.5	22	BCD
G063	10.5	90.0	3.0 -	5.0	4.5	22	BCD
G064	10.5	150.0	3.0 -	5.0	4.5	22	BCD
G065	10.5	210.0	3.0 -	5.0	4.5	22	BCD
G066	10.5	270.0	3.0 -	5.0	4.5	22	BCD
G067	10.5	330.0	3.0 -	5.0	4.5	22	BCD
G068	15.8	80.0	3.0 -	5.0	4.5	22	BCD
G069	10.0	30.0	3.0 -		4.5	22	BCD
G071	99999.9	0.0	3.5 -		4.5	13	BC
G072	11.1	30.0	3.5 -	5.5	4.5	13	BC
G073	11.1	90.0	3.5 -	5.5	4.5	13	BC

G074	11.1	150.0	3.5 - 5.5	4.5	13	BC
G075	11.1	210.0	3.5 - 5.5	4.5	13	BC
G076	11.1	270.0	3.5 - 5.5	4.5	13	BC
G077	11.1	330.0	3.5 - 5.5	4.5	13	BC
G081	99999.9	0.0	4.0 - 8.0	4.5	13	BC
G082	9.5	30.0	4.0 - 8.0	4.5	13	BC
G083	9.5	90.0	4.0 - 8.0	4.5	13	BC
G084	9.5	150.0	4.0 - 8.0	4.5	13	BC
G085	9.5	210.0	4.0 - 8.0	4.5	13	BC
G086	9.5	270.0	4.0 - 8.0	4.5	13	BC
G087	9.5	330.0	4.0 - 8.0	4.5	13	BC
G091	99999.9	0.0	5.0 - 10.0	5.0	13	BC
G092	10.5	30.0	5.0 - 10.0	5.0	13	BC
G093	10.5	90.0	5.0 - 10.0	5.0	13	BC
G094	10.5	150.0	5.0 - 10.0	5.0	13	BC
G095	10.5	210.0	5.0 - 10.0	5.0	13	BC
G096	10.5	270.0	5.0 - 10.0	5.0	13	BC
G097	10.5	330.0	5.0 - 10.0	5.0	13	BC
G101	99999.9	0.0	8.0 - 16.0	5.0	9	AB
G102	9.9	30.0	8.0 - 16.0	5.0	9	AB
G103	9.9	90.0	8.0 - 16.0	5.0	9	AB
G104	9.9	150.0	8.0 - 16.0	5.0	9	AB
G105	9.9	210.0	8.0 - 16.0	5.0	9	AB
G106	9.9	270.0	8.0 - 16.0	5.0	9	AB
G107	9.9	330.0	8.0 - 16.0	5.0	9	AB
GHO1	99999.9	0.0	2.0 - 4.0	3.0	8	AC_ne
GHO2	99999.9	0.0	3.5 - 5.5	3.0	8	AC_ne
GH03	99999.9	0.0	5.0 - 10.0	3.0	8	AC_ne
GHO4	99999.9	0.0	8.0 - 16.0	3.0	8	AC_ne
GV01	99999.9	0.0	0.5 - 1.5	3.0	10	D
GV02	99999.9	0.0	1.0 - 2.0	3.0	8	С
GV03	99999.9	0.0	1.5 - 2.5	3.0	8	С
GV04	99999.9	0.0	2.0 - 3.0	3.0	8	C
GV05	99999.9	0.0	2.0 - 4.0	3.0	8	С
GV06	99999.9	0.0	3.5 - 5.5	3.0	8	C

Table 4.2.2. GERESS beam table. Initial test beam set. The table shows name of beam, velocity (km/sec), azimuth (degrees), filter band (Hz), STA/LTA threshold, and configuration. The configuration is described with number of sensors and A, B, C or D-rings. Center A0 is always within the configuration. GH01 - GH04 are incoherent beams using horizontal components of the A2, D1, D4 and D7 three-component stations. GV01 - GV04 are incoherent beams using vertical components. This beam set has been in operation since 1990-294:03.

5 Maintenance Activities

5.1 Activities in the field and at the Maintenance Center

This section summarizes the activities in the field, at the Maintenance Center (NMC) Hamar and NDPC activities related to monitoring and control of the NORSAR, NORESS and ARCESS arrays.

Activities involve preventive and corrective maintenance, and in addition installation and modification of equipment in the field and at the Maintenance Center.

NORSAR

Visits were made to the arrays in connection with adjustment of channel gain and offset SP/LP. Adjustments of LP seismometer mass position (MP) and free period (FP) were made. Cables have been located/pointed out and also repaired/spliced. Subarrays have been visited in connection with loss of power. At the Well Head Vaults (WHVs) RA-5 amplifiers have been replaced. Communication lines have been tested and modems replaced.

NORESS

The NORESS array has been visited in connection with replacement of fiber optical transmitters on the Hub card (site C4). A water leakage was stopped in connection with C2 WHV. In June an AC power failure caused a visit to the central station (Hub). In September a new UPS (Uninterruptible Power Supply) system was installed.

ARCESS

Also here activities have been diverse. An air-conditioner in the central building at the array site has been replaced, and fiber optical transmitters have been replaced on fiber optical links. Fiber optical transmitters/receivers on the Hub 15 card were replaced (site C4). In addition, transmitters/receivers on a DHL 70 card were replaced (site D4). A GS- 13 seismometer was replaced (site D5).

Details are presented in Table 5.1.

Subarray/ area	Task	Date
NORSAR:	No visits	
NORESS:	Replaced fiber optical transmitters on Hub 15 card	5 April
NMC:	Tested/modified new equipment in connection with	April
	extension of the FINESA array	-
NDPC:	Daily check of NORSAR, NORESS, ARCESS and FINESA	April
	status	*
	Weekly calibration of NORSAR SP/LP instruments	
	Continuous measurement of Mass Position and Free	
	Period. Adjusted when outside tolerances	
NORSAR:		
02C	Located faulty SLEM power supply	3 May
01B	Meausrements revealed faulty cable SP02,04	7 May
01B	Cable work SP02,04	14 May
06C	Channel gain and DC offset on all SP/LP	19 May
	channels adjusted	
01B	Cable work SP02,04 terminated	22 May
04C	SP/LP checked	28 May
02C	Power failure stated; electricians from	30 May
	the local power plant had already arrived	
NORESS:	Stopped water leakage to the C2 Well Head	8,9,10
	Vault	May
	Reinstalled equipment, including seismometers	10 May
	C4 repaired	18 May
NDPC:	Daily check of NORSAR, NORESS, ARCESS and FINESA	May
	status	
	Weekly calibration of NORSAR SP/LP instruments	
	Continuous measurement of Mass Position and Free	
	Period	

Table 5.1 Activities in the field and the NORSAR Maintenance Center, including NDPC activities related to the NORSAR, NORESS, ARCESS and FINESA arrays, 1 April — 30 September 1990.

Subarray/	Task	Date
area		
NORSAR:		_
02B	A modem was replaced	8 June
	AC failure	19 June
	Gain adjusted on all channels (LTA)	
	DC offset adjusted on all channels	00 T
	"Old" modem reinstalled	22 June
04C	Lost AC power	1 June
06C	AC failure, 2 phases lost	28 June
NORESS:	AC failure	28 June
ARCESS:	Replaced air-conditioner	25,26
	Replaced optical transmitter at remote site	June
	Replaced all fiber optical links (to remote	
	sites)	
	Replaced fiber optical transmitters at the Hub	
NDPC:	15 card, site B1 and B3 Daily shark of NODEAR NODESS ADCESS and EINESA	Turna
NDPC:	Daily check of NORSAR, NORESS, ARCESS and FINESA	June
	status Weekly calibration of NORSAR SP/LP instruments	
	Continuous measurement of Mass Position and Free	
	Period	
	Adjustment of Mass Position and Free Period when	
	outside tolerances	
NORSAR:	ouside totelances	
02B	Visit in connection with loss of power	12 July
0215	SLEM reset	12 July 16 July
02C	Replaced FP/MP centering device EW seism.	4 July
	Cable splicing carried out SP05	10 July
04C	Comm. work in cooperation with NTA/Hamar	3,9 July
010	SP02,03 repair	17 July
	Repair of LP EW seismometer	18,19 July
	Gain and offset adjustments all channels SP/LP	20 July
06C	Installed a new RA-5 amplifier SP02	12 July
	Cable work carried out at site D5	16 July
ARCESS:	Replaced fiber optical transm./receiver on	24 July
	Hub 15 card, site 4	~~ <i>j</i>
	Reset "white box" communications unit	
	Replaced transm./receiver on DHL 68 card	
	site A0	

Table 5.1 (cont.)

Subarray/ area	Task	Date					
	Replaced DHL 70 card site D4 (vertical channel)						
	Replaced GS13 seismometer at site D5						
NDPC:	Daily check of NORSAR, NORESS, ARCESS and FINESA status	July					
	Weekly calibration of NORSAR SP/LP instruments						
	Continuous measurement of Mass Position and Free						
	Period						
	Adjustment of Mass Position and Free Period when						
	outside tolerances						
NORSAR:	Visit in connection with power loss	27 Aug					
02B	Cable work	27 Aug 27 Aug					
02D 04C							
04C 06C	Repaired SP cal. generator Cable pointed out						
FINESA:	NMC staff reinstalled data acquisition unit	31 Aug 20-26					
rmbsa.	New channels A0Z, A0Z low channel, A1NS, A1EW	Aug					
	installed	Aug					
NDPC:	Daily check of NORSAR, NORESS, ARCESS and FINESA	Aug					
	status						
	Weekly calibration of NORSAR SP/LP instruments						
	Continuous measurement of Mass Position and Free						
	Period						
	Adjustment of Mass Position and Free Period when						
	outside tolerances						
NORSAR:							
01A	Replaced RA-5, SP02	27 Sep					
	Channel gain all SP channels adjusted						
	MP/FP NS and EW LP seismometer adjusted						
04C	Replaced RCD (Remote Centering Device) NS	11 Sep					
	LP seismometer						
	Repaired improper connection in the EW data						
	circuit						
06C	Cable SP05 pointed out	7 Sep					
	Cable work SP04	10 Sep					
	Splicing of cable SP04,05	24 Sep					
NORESS:	Installed new UPS system	19-20 Sep					
	Installation and initialization	26 Sep					

Table 5.1 (cont.)

Subarray/	Task	
area		
NDPC:	Daily check of NORSAR, NORESS, ARCESS and FINESA status	
	Weekly calibration of NORSAR SP/LP instruments.	
	Continuous measurement of Mass Position and Free Period	
	2 0110 4	
	Adjustment of Mass Position and Free Period when outside tolerances	

Table 5.1 (cont.)

5.2 Array status

As of 30 September 1990 the following NORSAR channels deviated from tolerances.

01A 01 8 Hz filter 02 8 Hz filter 04 30 dB attenuator

O.A. Hansen

6 Documentation Developed

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L.B. Loughran

7 Summary of Technical Reports / Papers Published

7.1 Detection and yield estimation studies

1. Yield estimation using Lg recordings

Over the past several years, extensive research has taken place at NORSAR to develop and evaluate the RMS Lg estimation technique for underground nuclear explosions. Some of the most recent results have been documented by Ringdal and Marshall (1989) and Hansen, Ringdal and Richards (1990).

These studies have so far concentrated on the Shagan River (Semipalatinsk) test site, using data from stations in Norway, Germany, USSR and China (Fig. 7.1.1). By using NORSAR as a reference system, and plotting observed RMS Lg for other stations against NORSAR values, it has been found that the standard deviations of the residuals are consistently as low as 0.03 magnitude units, as shown for selected stations in Fig. 7.1.2. Furthermore, comparing two of the stations with lowest Lg detection threshold (GAM and ARU in the Soviet Union), we have found that this consistency appears to span two full orders of event magnitude, down to approximately $m_b = 4.0$ (Hansen *et al*, 1990).

A possibility to compare the RMS Lg magnitudes to published yields for Semipalatinsk explosions has now emerged with the recent publication by Soviet scientists quoting yield estimates for a number of such explosions (Bocharov *et al*, 1989; see also Vergino, 1989a,b). We have made an effort to conduct detailed analysis of available NORSAR Lg data for the explosions in this data set. Since NORSAR is located at more than 4000 km distance from Semipalatinsk, only explosions of more than 10 kt yield will usually provide sufficient SNR for Lg measurements at this station, and even so, it must be noted that at these lower yields, the estimated RMS Lg is less precise than at yields exceeding 50 kt.

Table 7.1.1 gives the NORSAR Lg magnitudes obtained in these analyses. The table comprises altogether 8 explosions from both the Shagan River (Balapan), Degelen Mountains and Konystan (Murzhik) subareas. The NORSAR data for the four largest of these explosions have been previously presented in Ringdal (1989).

Fig. 7.1.3 (top part) shows a plot of NORSAR M(Lg) versus published yields for these 8 explosions. For comparison, the bottom part of Fig. 7.1.3 shows world-wide m_b (UK values as quoted by Vergino, 1989a) versus yield for the same 8 events. The slope in each plot has been restricted to 0.75, and the standard deviation in the vertical direction is 0.043 for M(Lg) and 0.081 for m_b versus log yield. We note that this data set is too small to allow any confident estimate of the accuracy in estimating yield from M(Lg), especially in view of the aforementioned uncertainty in M(Lg) values for the smaller explosions. Nevertheless, the figure would appear to confirm the potential of RMS Lg as a stable estimator of yields for fully coupled explosions from this region, and indicates that even single station M(Lg) is better correlated to log(yield) than is world-wide m_b .

2. P-wave detectability studies

Ringdal (1990) has conducted a study of the NORESS array detection capability for Semipalatinsk explosions, both in terms of m_b and yield (Bocharov *et al*, 1989). In terms of NORESS m_b , the 50 per cent detection threshold is estimated at $m_b = 3.7 \pm 0.1$. A noteworthy feature, illustrated in Fig. 7.1.4, is the large difference in NORSAR m_b bias (S) for the subregions Shagan River (S ≈ 1.0) and Degelen/Konystan (S ≈ 0.4). In terms of world-wide m_b , the estimated NORESS detection threshold, at the 50 per cent level, thus becomes $m_b = 2.7$ and $m_b = 3.3$ for these subareas, respectively.

Fig. 7.1.5 shows NORESS m_b values (measured at the NORSAR seismometer 06C02 which is co-located with the present NORESS center site) versus log yield for 6 low-yield nuclear explosions (the only ones in Bocharov *et al* (1989) with available data that did not exceed NORSAR's dynamic range). As before, we have used a restricted slope of 0.75 in the magnitude-log yield relationship, and fitted a straight line with this slope to the observed data. The NORESS beam threshold range (plus/minus two standard deviations) is shown as dotted horizontal lines.

Fig. 7.1.5 indicates that, given similar coupling conditions and noise levels as in our data base of 6 explosions, Semipalatinsk explosions of yields at 0.1 kt would be expected to produce detectable signals at NORESS. We note that the 6 reference explosions are all from Degelen or Konystan. In view of the previous discussions, the detectability for Shagan River explosions would be expected to be even better.

In Fig. 7.1.6, we plot NORESS, ARCESS, FINESA and GERESS recordings of an $m_b = 5.7$ nuclear explosion at Novaya Zemlya. The figure shows an unfiltered, single sensor trace for each array, and the signal-to-noise rato on the best array beam (STA/LTA as computed by the online detector) is given in the figure caption. ARCESS has a strong S-phase detection, and there is some S-wave energy visible also for the three other arrays. The Lg phase is not visible on these unfiltered recordings, but in the best filter band, the energy in the Lg window still exceeds significantly the pre-P noise.

From Fig. 7.1.6 it is seen that the P-wave detection capability for Novaya Zemlya explosions is excellent for NORESS, FINESA and ARCESS, in particular the latter. Thus, ARCESS SNR for the event shown was 8383 on the array beam in the filter band 3-5 Hz. This is more than 3 orders of magnitude above the operational threshold, and we note that similar SNR has been observed for the other Novaya Zemlya explosions of similar size recorded at ARCESS (only 4 such events have been recorded since the array came into operation). While this is too limited a data base to give a reliable threshold estimate, a straight extrapolation would indicate that the ARCESS threshold at this site is well below $m_b = 3.0$. NORESS and FINESA also appear to have thresholds close to $m_b = 3.0$, whereas GERESS has a lower detectability for this test site.

3. Conclusions and Recommendations

Our studies confirm that Lg magnitude estimates of Semipalatinsk explosions are remarkably consistent between stations widely distributed in epicentral distance and azimuth. It thus appears that a single station with good signal-to-noise ratio can provide M(Lg) measurements with an accuracy (one standard deviation) of about 0.03 magnitude unit. It is noteworthy that this accuracy is consistently obtained for a variety of stations at very different azimuths and distances, even though the basic parameters remain exactly as originally proposed by Ringdal for NORSAR recordings (0.6–3.0 Hz bandpass filter, RMS window length of 2 minutes, centered at a time corresponding to a group velocity of 3.5 km/s). Moreover, the Lg phase shows considerable promise for use in yield determination, although more data will be needed before the accuracy of Lg-estimated yields can be firmly established.

The excellent detection capability of the regional arrays in northern Europe have been confirmed by case studies, comprising a detailed evaluation of the NORESS capability for Semipalatinsk explosions, and preliminary observations of ARCESS detection of Novaya Zemlya explosions.

Further work will be directed toward additional expansion of these studies, in particular analyzing new data as they become available, and pursuing our analysis of Novaya Zemlya recordings at regional arrays as well as other available stations.

F. Ringdal

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Date	Region	m _b	NORSAR	Yield
			M(Lg)	(kt)
11/30/69	Shagan (TZ)	6.048	6.043	125
04/25/71	Degelen	6.076	5.862	90
06/06/71	Konystan	5,526	5.44	16
10/09/71	Konystan	5.371	$5.25^{*)}$	12
10/21/71	Konystan	5.580	5.54	23
02/10/72	Shagan (NE)	5.370	5.37	16
11/02/72	Shagan (SW)	6.224	6.118	165
12/10/72	Shagan (NE)	5.996	6.095**)	140

*) Low precision due to low SNR

**) Adjusted for interfering explosion

Table 7.1.1. Parameters of eight explosions analyzed in this study. Yield estimates are from Bocharov *et al* (1989), and the m_b values are the "UK m_b " listed in Vergino (1989a).

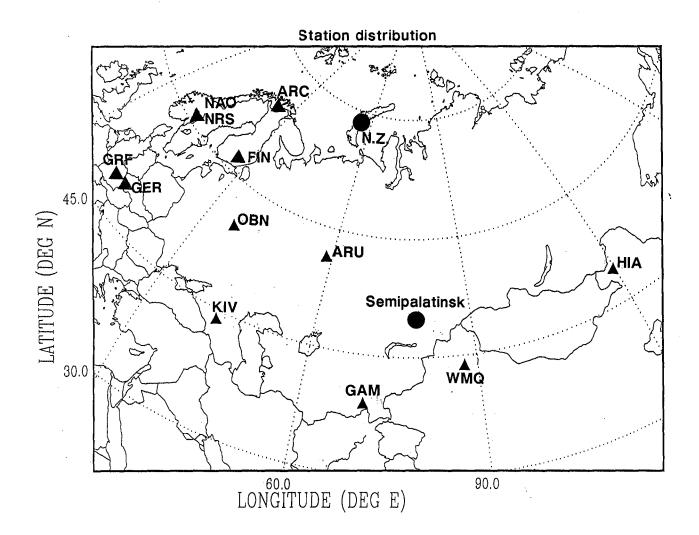


Fig. 7.1.1. Map showing the location of stations analyzed in this study (triangles). The two main USSR test sites (Novaya Zemlya and Semipalatinsk) are marked as filled circles.

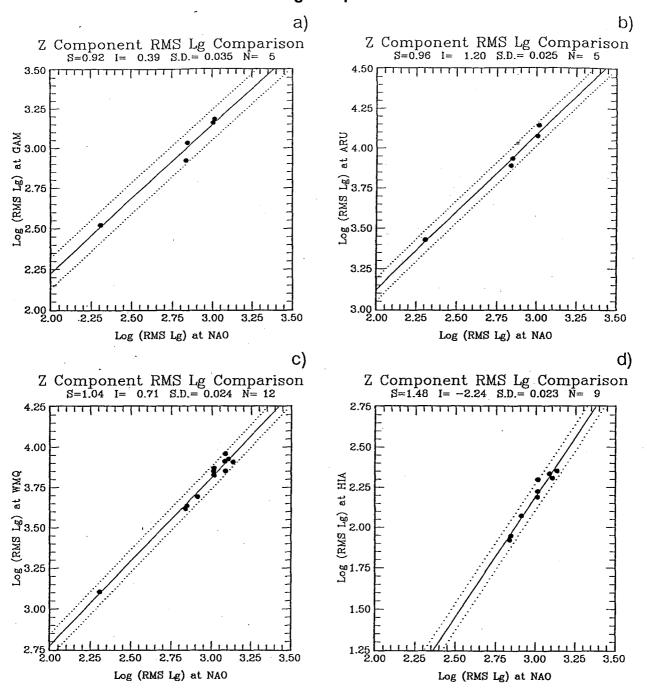


Fig. 7.1.2. Examples of observed correlations between RMS Lg at NORSAR and selected stations in the USSR and China. Note the excellent consistency in all of the plots.

RMS Lg comparison

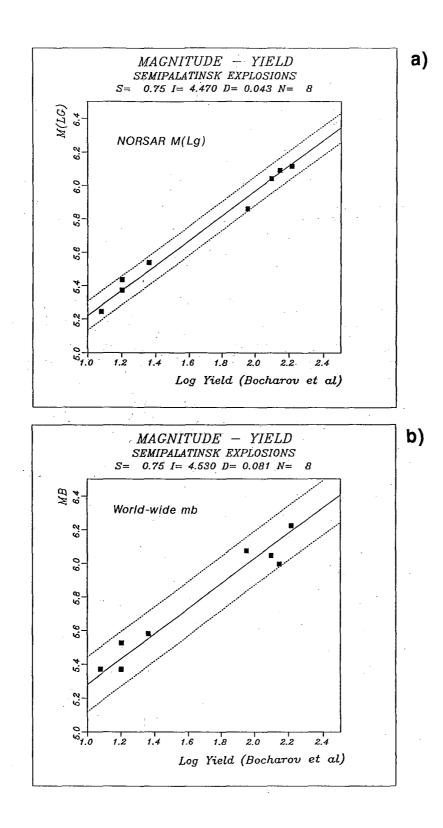


Fig. 7.1.3. Magnitude-yield relationships for 8 nuclear explosions at Semipalatinsk, with yields provided by Bocharov *et al* (1989): a) NORSAR M(Lg) versus log(yield) and b) world-wide m_b versus log(yield). The slopes of the straight lines have been restricted to 0.75. Note that the NORSAR values show significantly less scatter.

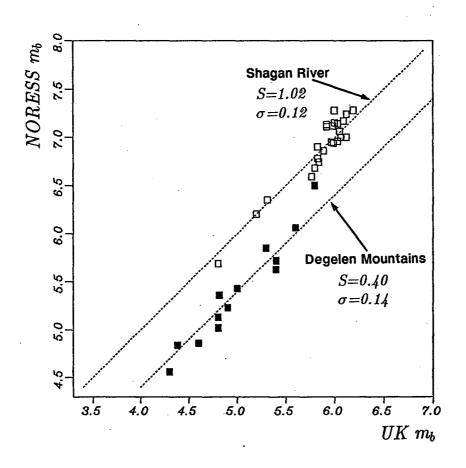


Fig. 7.1.4. Comparison of NORESS and world-wide m_b (as calculated at Blacknest, United Kingdom) for Semipalatinsk explosions. Note the difference in average m_b bias between events from Shagan River (1.0 m_b units) and Degelen Mountains (0.4 m_b units). The straight lines on the plot have a restricted slope of 1.00.

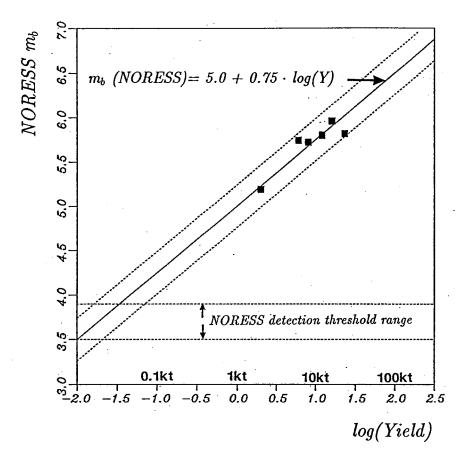
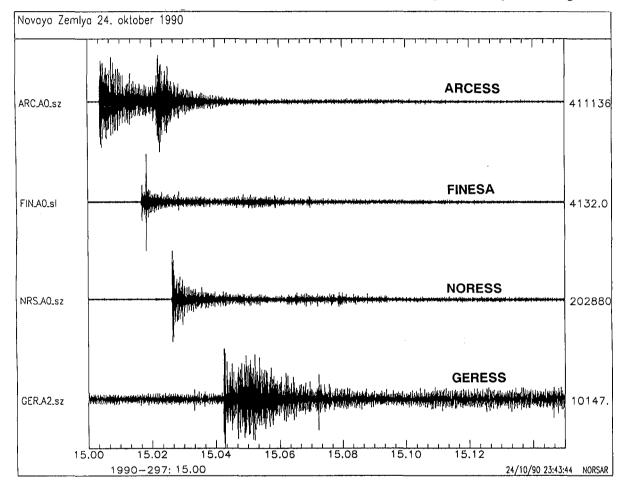
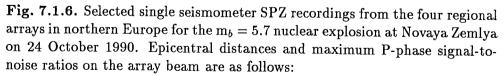


Fig. 7.1.5. Observed m_b versus yield (Bocharov *et al*, 1989) for six Semipalatinsk nuclear explosions listed in Table 7.1.1. The straight line has been fitted using a restricted slope of 0.75. The m_b values are based on NORSAR seismometer 06C02, located at the present NORESS center site. The estimated range of the NORESS m_b detection threshold is indicated (see text for details).



Novaya Zemlya nuclear explosion 24 October 1990 - Regional array recordings



ARCESS 1110 km, SNR = 8383; FINESA 1780 km, SNR = 2189 NORESS 2270 km, SNR = 2478; GERESS 3380 km, SNR = 105

7.2 Initial results from real-time processing of GERESS array data

Introduction

The GERESS array (Harjes, 1990) represents the most recent addition to the network of regional seismic arrays in Europe. GERESS, which is located in the Bavarian Forest area in southern Germany, has a geometry similar to that of NORESS in southern Norway and ARCESS in northern Norway, but with a slightly enlarged instrument spacing (Fig. 7.2.1). Thus the diameter of GERESS is 4 km, compared to 3 km for the two arrays in Norway.

Real-time data from GERESS are transmitted continuously both to Bochum, Germany (by land line), and to the NORSAR Data Processing Center (NDPC) at Kjeller (by satellite). At NDPC, the data are currently subjected to continuous real-time detection processing, using the RONAPP algorithm (Mykkeltveit and Bungum, 1984). In the near future, these data will also be incorporated into the Intelligent Monitoring System (IMS) (Bache *et al*, 1990).

GERESS real-time processing

The initial processing of GERESS data is conducted at NDPC using a beam set essentially identical to that being used for NORESS and ARCESS data (see Subsection 3.4). Although several modifications will undoubtedly be desirable after more experience is gained, it is still of interest to observe how a "generic" parameter set performs when applied to a regional array in a new geological environment. Below, we give some initial examples from this processing.

Table 7.2.1 shows excerpts from the automatic GERESS phase detection list for day 293 (23 October 1990). For each phase, the detection time, beam number, SNR, phase velocity and azimuth are listed, together with a number of attributes used in further characterization of the detected phase.

In Fig. 7.2.2 we show an automatically generated event plot (Fyen, 1989) for one of the located events during the time period covered by the detection list in Table 7.2.1. This event is located in the Lubin mining district in Poland, at a distance of 344 km from GERESS, and is probably one of a large number of rockbursts known to occur in that region (Gibowics, 1987). We note that this event was too small to be detected by either NORESS, ARCESS or FINESA.

Fig. 7.2.3 shows GERESS automatic output plot from the P-wave detection of the Novaya Zemlya explosion 24 October 1990 ($\Delta = 30.4$ degrees). The phase velocity is indicative of a teleseismic signal, and the estimated azimuth is consistent with the actual epicenter. GERESS SNR is 105 on the array beam, which is naturally lower than for the three other arrays, all of which are within regional distances from Novaya Zemlya. An interesting feature of the GERESS recordings of this event is a very sharp PcP detection at 2 min 59.5 seconds after P (Fig. 7.2.4). The time differential between P and PcP gives a very sharp constraint on the epicentral distance, in particular when the phase onset times can be read as precisely as in this case. Thus, given appropriate calibration, very useful location information could be derived.

Conclusions

Our initial experience shows that real-time processing of GERESS data will form a very valuable contribution to the regional array monitoring research network. So far, it appears that many new events in southern Europe within 500 km distance from GERESS will be added, and GERESS data will provide further constraints on the events detected and located by more than one array. The teleseismic potential of GERESS is also quite promising.

J. Fyen

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		4 0	2 6 moto	200 5 0 06 4	1 00	052.2	172 0 32 07	-1.00 - 1.00 - 1.00 - 1.00
323 293:12.43.29.700	1.10 G053	4.8		298.5 0.06 4	4.02	953.3	173.9 A3_sz	
324 293:12.43.39.750	1.25 GV01	3.8	12.9 P	191.0 0.17 1	0.56	76.5	404.7 C1_sz	0.59 2.06 80.33 4.28
325 293:12.45.10.987	0.31 G084	7.7		310.0 0.07 4	6.31	2650.3	505.5 D5_sz	-1.00 -1.00 -1.00 -1.00
326 293:12.45.19.300	1.20 GV01	7.2	4.3 S	201.9 0.11 3	0.72	289.1	658.7 D5_sz	-1.00 - 1.00 - 1.00 - 1.00
327 293:12.47.07.050	0.75 G043	15.5		124.5 0.05 4	3.16	1472.7	268.3 C5_sz	-1.00 - 1.00 - 1.00 - 1.00
328 293:12.47.16.475	1.02 GV06	3.2	1.9 nois	310.0 0.09 3	4.79	1713.6	609.2 C5_sz	-1.00 - 1.00 - 1.00 - 1.00
329 293:12.47.39.300	1.00 G011	7.2	14.7 P	202.8 0.29 1	1.31	74.5	340.9 C5_sz	0.42 1.34 8.20 4.21
330 293:12.56.39.725	0.98 GV01	6.0	35.9 P	346.7 0.54 1	1.04	118.7	498.4 A3_sz	0.54 3.06 89.38 3.18
331 293:12.58.45.675	0.22 GH03	3.9	2.9 nois	45.7 0.07 3	7.74	2095.2	299.4 C1 ⁻ sz	-1.00 -1.00 -1.00 -1.00
332 293:12.58.50.300	0.50 G032	4.5	37.7 P	147.3 0.09 3	3.30	167.0	85.9 C1 ⁻ sz	-1.00 - 1.00 - 1.00 - 1.00
333 293:13.01.31.481	1.12 G103	6.8	2.8 nois	339.3 0.04 4	7.74	2619.1	659.5 A0 sz	0.34 1.85 86.29 33.93
334 293:13.04.21.800	1.30 G034	7.3		145.4 0.07 3	2.13	477.6	126.0 A3 sz	-1.00 - 1.00 - 1.00 - 1.00
335 293:13.04.27.650	0.65 G021	4.7	3.2 S	3.6 0.05 4	1.94	491.2	118.1 A3 sz	-1.00 - 1.00 - 1.00 - 1.00
336 293:13.11.29.750	0.55 G036	7.3		140.6 0.08 3	2.14	349.7	134.6 A3 sz	-1.00 -1.00 -1.00 -1.00
337 293:13.11.40.075	1.12 GV01	3.1	15.6 P	30.5 0.56 1	0.79	164.7	335.2 A3 sz	0.60 3.14 88.70 5.40
	0.17 GH04	3.7		31.0 0.05 4	8.29	689.6	256.7 A0 sz	0.19 2.25 64.50 5.08
338 293:13.15.50.331	0.52 G033	4.6		$150.1 \ 0.10 \ 4$	2.51	398.6	77.3 D8 sz	-1.00 -1.00 -1.00 -1.00
339 293:13.22.49.575				$124.1 \ 0.47 \ 1$				-1.00 -1.00 -1.00 -1.00
340 293:13.27.39.625	1.07 GV01	5.6	11.6 P		0.93	45.0	464.5 A3_sz	
341 293:13.27.59.675	1.32 GV01	3.7	4.0 S	343.5 0.48 1	0.64	195.2	334.5 B3_sz	-1.00 -1.00 -1.00 -1.00
342 293:13.28.19.875	1.12 GV01	3.6		150.7 0.47 1	0.86	72.8	329.6 B3_sz	-1.00 - 1.00 - 1.00 - 1.00
343 293:13.30.14.306	0.59 GH04	4.2	3.1 S	333.1 0.04 4	5.64	1212.3	388.4 A3_sz	0.30 0.96 31.26 47.69
344 293:13.33.19.525	1.27 G034	17.7	8.0 Pgn	130.7 0.39 1	2.60	315.6	260.1 A0_sz	0.75 0.50 45.92 75.59
345 293:13.33.29.425	1.17 G044	6.3	8.0 Pgn	150.7 0.40 1	2.95	646.6	300.4 A0_sz	-1.00 - 1.00 - 1.00 - 1.00
346 293:13.36.05.362	0.44 G087	11.2	4.2 S	106.5 0.06 4	6.44	2133.4	697.2 A3_sz	-1.00 - 1.00 - 1.00 - 1.00
347 293:13.36.15.700	1.10 G051	4.9		149.1 0.06 4	3.88	971.7	137.3 A3_sz	0.16 0.80 65.16 87.88
348 293:14.18.12.350	0.95 G059	12.1	7.5 Pgn	352.9 0.19 1	2.82	643.5	190.8 A0 sz	0.73 0.90 47.35 54.70
349 293:14.18.34.725	1.38 G065	8.9	4.2 SN	354.6 0.14 3	3.25	1872.5	308.1 A0 sz	0.67 1.82 85.96 10.60
350 293:14.18.38.950	1.25 GV06	4.4	4.3 S	0.7 0.12 3	3.93	1300.8	691.4 A0 sz	-1.00 - 1.00 - 1.00 - 1.00
351 293:14.25.06.875	0.92 G044	9.4	3.0 S	142.7 0.06 3	3.05	861.0	197.0 D2 sz	-1.00 - 1.00 - 1.00 - 1.00
352 293:14.25.10.025	1.67 GV02	4.4	2.7 nois	149.5 0.06 3	1.86	406.4	279.0 D2 sz	-1.00 - 1.00 - 1.00 - 1.00
353 293:14.25.36.925	1.38 G055	6.1		267.7 0.06 4	4.18	645.3	128.0 D7 se	0.20 1.14 78.45 51.94
354 293:14.46.24.550	1.95 GV02	3.1	28.4 P	106.1 0.16 3	1.89	34.9	93.3 B3 sz	-1.00 - 1.00 - 1.00 - 1.00
355 293:14.49.39.275	1.02 G058	5.6	3.2 S	167.3 0.06 3	3.47	472.1	95.7 A3 sz	-1.00 -1.00 -1.00 -1.00
356 293:14.50.26.100	1.20 G034	4.6	3.8 S	339.4 0.06 4	2.46	359.0	77.7 D2 sz	-1.00 - 1.00 - 1.00 - 1.00
357 293:14.51.39.350	1.35 GV01	7.4		164.6 0.30 1	0.45	96.4	572.0 C5 sz	-1.00 -1.00 -1.00 -1.00
358 293:14.53.21.975	0.82 G051	5.0		226.2 0.07 4	3.96	466.9	92.2 C1_sz	0.17 1.21 72.27 33.76
359 293:14.54.31.281	0.82 G104	7.4	3.2 SN	160.4 0.04 4	8.96	3746.4	1052.4 A3 sz	0.27 2.95 89.00 4.00
360 293:14.55.49.975	0.62 G035			274.0 0.05 4	2.69	537.3	110.2 D2 sz	-1.00 -1.00 -1.00 -1.00
		6.9						
361 293:14.57.11.050	1.05 G035	8.2		140.7 0.07 3	1.98	713.8	133.3 C5_sz	-1.00 -1.00 -1.00 -1.00
362 293:14.57.19.325	1.48 G035	9.9		153.5 0.05 3	2.15	881.3	225.2 C5_sz	-1.00 -1.00 -1.00 -1.00
363 293:14.57.24.750	0.95 GV02	3.6		62.5 0.07 3	1.59	391.9	374.2 C5_sz	-1.00 -1.00 -1.00 -1.00
364 293:14.57.52.125	0.88 GV02	3.0	3.0 S	326.0 0.10 4	1.55	179.4	246.1 D5_sz	-1.00 - 1.00 - 1.00 - 1.00
365 293:15.01.53.150	0.95 G034	5.3	3.0 S	153.8 0.08 3	2.18	383.9	79.6 A3_sz	-1.00 - 1.00 - 1.00 - 1.00
366 293:15.07.29.725	0.88 G035	8.7		284.7 0.05 4	2.47	846.6	144.6 D2_sz	0.35 1.61 82.97 53.64
367 293:15.09.02.475	1.12 G049	5.6	3.8 S	341.7 0.07 3	3.17	416.6	103.9 A3_sz	-1.00 - 1.00 - 1.00 - 1.00
368 293:15.11.04.450	0.65 G042	5.1	3.1 S	254.3 0.05 4	2.82	1218.1	103.7 A3_sz	-1.00 - 1.00 - 1.00 - 1.00
369 293:15.11.31.775	0.82 G056	6.6	35.3 P	223.5 0.06 4	3.84	118.4	170.2 A3_sz	0.30 1.61 87.77 22.09
370 293:15.18.34.575	0.52 G038	6.0	2.8 nois	147.0 0.09 3	2.08	762.8	86.8 C1 sz	0.20 0.77 83.64 79.27
371 293:15.18.39.225	1.07 G052	6.5	2.6 nois	105.5 0.09 3	4.59	647.0	147.5 D5 sz	0.17 1.60 87.76 4.35
372 293:15.45.33.575	0.52 G033	707.5		295.2 0.03 4	2.26	26191.2	11225.5 A3 sz	0.26 1.46 83.60 34.12
373 293:16.08.43.925	2.17 G011	4.5		348.1 0.19 3	1.08	320.3	183.4 D9 sz	0.39 2.50 89.11 21.66
374 293:16.12.06.075	1.23 G036	5.1	12.4 P	258.1 0.09 4	2.32	122.2	99.8 D8 sz	-1.00 - 1.00 - 1.00 - 1.00
375 293:16.28.21.575	0.52 G049	4.8		146.9 0.13 3	2.51	343.0	87.3 D5 sz	0.57 0.87 39.37 48.97
376 293:16.28.25.875	2.12 GV06	5.3	6.8 Pgn	33.3 0.19 3	4.82	880.2	566.5 D5 sz	0.59 0.94 41.68 50.28
377 293:16.28.35.800	0.50 G057	4.8	6.8 Pgn	32.3 0.21 2	3.71	417.6	147.1 D5 sz	-1.00 -1.00 -1.00 -1.00
378 293:16.29.10.675	0.52 GH01	6.2	4.6 S	40.1 0.20 3	2.88	2349.6	1100.9 B3 sz	0.22 1.45 71.53 14.51
510 235.10.23.10.075	0.52 0001	0.2	7.0 5	TU.L U.ZU J	2.00	2347.0	1100.9 03_92	1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.

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Table 7.2.1. (Page 1 of 2)

379 293:16.29.14.425	1.57 GV02	4.0	3.3 LG	31.5 0.31 2	1.47	1019.1	508.0 B3 sz	0.55 1.41 79.68 77.38
380 293:16.29.18.375	1.62 GV02	3.1	4.4 S	24.5 0.32 1	1.59	1159.0	505.8 B3 sz	-1.00 - 1.00 - 1.00 - 1.00
381 293:16.29.19.725	0.98 GV01	5.6	3.5 S	19.1 0.23 2	1.51	764.1	915.5 A0 sz	-1.00 -1.00 -1.00 -1.00
382 293:16.35.18.525	2.48 GV01	3.4	29.9 P	277.5 0.14 3	0.83	114.9	304.4 D4 sn	-1.00 - 1.00 - 1.00 - 1.00
383 293:17.12.59.500	1.20 GV01	5.6	26.4 P	146.9 0.45 1	1.08	158.6	681.5 B3 sz	-1.00 -1.00 -1.00 -1.00
384 293:17.15.23.700	0.90 G093	7.1	6.3 Pgn	113.5 0.05 4	7.43	1175.0	453.0 A3 sz	-1.00 -1.00 -1.00 -1.00
385 293:17.36.39.750	0.95 GV01	7.6	5.0 S	206.3 0.14 4	1.03	286.6	902.8 B2 sz	-1.00 - 1.00 - 1.00 - 1.00
386 293:17.48.42.350	0.95 G049	5.3	4.4 S	145.0 0.06 3	3.27	506.9	100.5 A3_sz	-1.00 - 1.00 - 1.00 - 1.00
387 293:17.51.19.950	0.75 GV01	6.0	9.4 Pqn	315.4 0.24 1	0.57	94.2	460.0 A0 sz	-1.00 - 1.00 - 1.00 - 1.00
388 293:18.38.37.850	3.15 GV01	3.4	8.2 Pgn	187.5 0.42 1	0.86	44.2	400.8 C1 ⁻ sz	0.25 1.78 88.86 8.36
389 293:18.46.16.650	1.45 G042	4.9		138.2 0.14 3	3.05	597.5	88.7 B5 sz	-1.00 - 1.00 - 1.00 - 1.00
390 293:18.48.49.825	0.48 G071	5.0	3.3 S	121.9 0.05 4	4.77	435.7	166.8 A3 sz	-1.00 - 1.00 - 1.00 - 1.00
391 293:18.49.08.950	1.55 GV04	3.1	2.7 nois	140.1 0.08 3	2.37	294.5	212.6 C5 sz	-1.00 - 1.00 - 1.00 - 1.00
392 293:18.49.19.525	0.77 G054	5.2	13.0 P	290.4 0.06 4	4.01	86.6	103.2 D5 sz	-1.00 - 1.00 - 1.00 - 1.00
393 293:18.51.32.550	1.55 G053	5.6	2.8 nois	321.8 0.07 4	3.68	521.0	101.3 A0 sz	0.54 2.47 85.13 18.21
394 293:18.56.19.125	1.57 GV01	4.0	4.8 S	294.2 0.16 3	1.02	369.7	423.5 D2 sz	-1.00 - 1.00 - 1.00 - 1.00
395 293:19.08.01.150	1.55 GV02	3.1	2.2 nois	129.2 0.08 3	1.68	283.3	186.2 D2 ⁻ sz	-1.00 -1.00 -1.00 -1.00
396 293:19.08.39.500	1.20 GV01	6.4	8.3 Pgn	162.1 0.42 1	0.63	130.4	774.7 D5 sz	-1.00 -1.00 -1.00 -1.00
397 293:19.10.00.175	0.82 GV01	3.8	5.8 S	23.0 0.32 1	0.64	251.0	385.7 B4 sz	-1.00 -1.00 -1.00 -1.00
398 293:19.19.29.750	0.55 G021	4.6	16.4 P	132.7 0.06 4	1.98	176.5	102.9 A3 sz	-1.00 -1.00 -1.00 -1.00
399 293:19.21.18.775	2.42 GV01	3.3	5.8 S	185.7 0.29 1	0.87	324.8	368.5 D8_sz	-1.00 -1.00 -1.00 -1.00
400 293:19.31.39.900	1.10 GV01	3.9	7.1 Pgn	167.2 0.26 1	0.85	64.1	377.5 D2_sz	-1.00 -1.00 -1.00 -1.00
401 293:19.40.59.925	1.07 GV01	3.3	22.8 P	14.2 0.44 1	0.93	65.9	314.0 A3 <u>s</u> z	1-1.00 -1.00 -1.00 -1.00
402 293:19.48.59.775	0.92 GV02	4.0	2.2 nois	29.2 0.08 3	1.97	211.5	213.5 C1_sz	-1.00 -1.00 -1.00 -1.00
403 293:20.07.57.375	2.92 G011	5.1	34.3 P	310.0 0.17 3	1.06	241.5	234.1 D2_sz	-1.00 - 1.00 - 1.00 - 1.00
404 293:20.10.40.450	0.55 GV05	3.3		146.0 0.13 3	2.16	285.6	256.6 C1 <u></u> sz	-1.00 - 1.00 - 1.00 - 1.00
405 293:20.18.48.525	0.77 G065	5.0		218.7 0.06 4	4.11	363.7	89.4 D7_sn	-1.00 - 1.00 - 1.00 - 1.00
406 293:20.20.40.025	0.98 GV02	3.0	6.1 Pgn	359.9 0.08 4	1.79	55.2	173.2 D9_sz	0.27 1.47 85.01 40.82
407 293:20.51.39.850	0.75 G053	4.8	3.2 SN	266.1 0.06 3	3.93	252.0	57.4 D2_sz	0.28 1.81 86.86 14.22
408 293:21.08.19.750	1.25 GV01	3.6	16.4 P	179.1 0.53 1	0.57	135.1	387.1 D8_sz	-1.00 - 1.00 - 1.00 - 1.00
409 293:21.15.19.675	1.32 GV01	3.4	13.8 P	228.6 0.15 3	0.48	63.1	325.8 D5_sz	-1.00 - 1.00 - 1.00 - 1.00
410 293:21.27.39.925	1.07 GV01	4.2	12.1 P	278.5 0.32 3	0.88	170.9	317.6 A3_sz	0.28 2.03 84.67 15.54
411 293:22.09.09.175	2.62 G021	5.1	48.6 P	329.0 0.32 2	1.33	179.7	110.9 A0_sz	-1.00 -1.00 -1.00 -1.00
412 293:22.40.00.225	0.77 GV01	4.0	4.8 S	317.6 0.33 1	0.96	229.5	341.6 B3_sz	-1.00 -1.00 -1.00 -1.00
413 293:23.17.59.375	1.62 GV01	3.1	8.8 Pgn	227.4 0.37 1	0.96	82.7	237.1 D5_sz	-1.00 -1.00 -1.00 -1.00
414 293:23.21.19.750	1.25 GV01	3.2	4.6 S	315.9 0.49 1	0.75	203.8	242.9 A3_sz	-1.00 -1.00 -1.00 -1.00
415 293:23.49.17.775	3.23 GV01	3.2	10.4 P	85.5 0.10 3	0.86	65.2	326.6 D9_sz	-1.00 -1.00 -1.00 -1.00

Table 7.2.1. Automatic event processor detection log for the GERESS array. From left to right the columns give arrival identification number, estimated onset time, difference in seconds between STA/LTA trigger time and onset time, beam name, SNR, velocity in km/sec, phase name, azimuth, broadband FK relative coherence measure and quality of FK (1=good), frequency in Hz of estimated maximum amplitude of the phase, phase maximum amplitude in uncorrected digital counts, STA. The next column with channel names gives, in case of many data gaps, the name of one channel that due to gaps/spikes, etc., may have contributed to a false detection. The four last numbers are result of three-component polarization analysis, and give rectilinearity, horizontal/vertical ratio, angle of incidence 1 and 3. (Page 2 of 2)

11.0

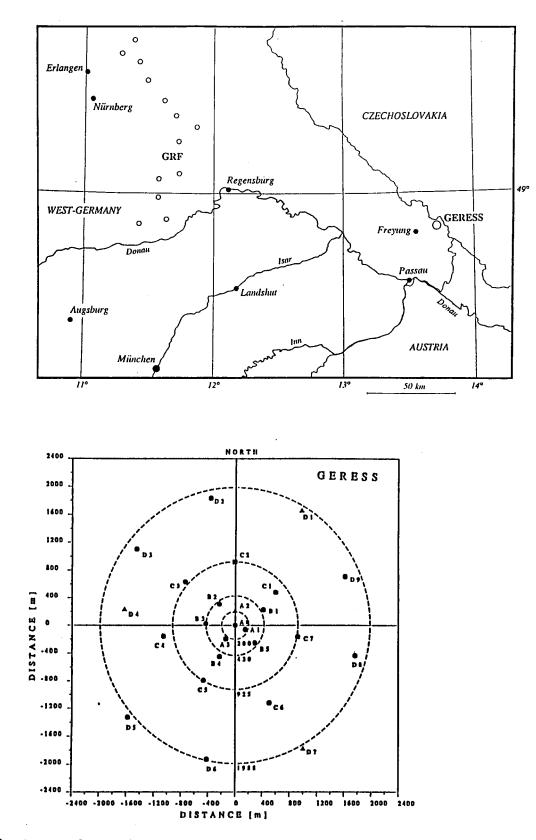


Fig. 7.2.1. Geographical location and geometry of the GERESS array in Germany (after Harjes, 1990).

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EPY 100 100	0-203.1	6 27 35 006	Lat 51.40 Lon 16.37 Azi 32.56 Dst 344.31 A 1282.0 , 1282.0 f 1.47 ML 3	01
FKX 376 Pha	se PN at	1990-293;	16.28.25.875 vel 6.80 azi 33.30 rpw 0.190 g 3 a 1282.0 f 4.82 fband 3.5	0 5.50
		PNp		
GER_AO_sz				13193.
GER_B1_sz	,##1\$******			1785.2
GER_B2.sz	e hel nit find the state of			2092.5
GER_B3_sz				10456.
GER_B4_sz	(14-1-14)	Manifer alls and some shift of		1960.6
GER_B5_sz	*****		.	3207.2
GER_C1_sz	-14,00 11111-1-14		le be a state production to be a state and the manual state and the state of a second state with the second state and the state of the	1961.5
GER_C2_sz	 	fohnet har ast		1882.0
GER_C3_sz		alithe forme des and the alithe ali	••••••••••••••••••••••••••••••••••••••	3205.2
GER_C4_sz	<u>Herden biskoppisi</u>			2284.7
GER_C5_sz	114			2133.5
GER_C6_sz	****		₩₩ <u>₽₽</u> ₩₩₩ <mark>₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩</mark>	2514.3
GER_C7_sz			the all and a finance and an analysis and and and any strength of the second second and and any strength and a second	1733.3
GV06	++			1385.4
GV02			16.30 16.31 16.32 16.33	835.86
GERESS	6.28 <u>19</u> 9	16.29 0-293:16.		:58 NORSAR

Fig. 7.2.2. Automatically generated event plot for GERESS. The traces shown are a selection of single instruments filtered in the band 3.5-5.5 Hz. The bottom two traces are the P- and S-beams using the velocities and azimuths determined by broadband F-K analysis. (The S-beam, which is the lowermost trace, is filtered in the band 1.0-2.0 Hz). The time window is 6 minutes.

	am G032 At 1990-297:15.04.13.725 snr 105.2 19.70 ozi 42.30 rpw 0.510 q 1 o 3792.1 f 2.28	0 3.fband 1.50 3.50	
GER.A0.sz			7938.8
GER_C4_sz			6621.4
GER_C5_sz		- MMM Manna Markan Markan	9848.3
GER_C6_sz	· · · · · · · · · · · · · · · · · · ·	-MMMmmmmmmmmmmmmmmmmmmmmmmmmmmmmmmmmmm	8522.4
GER_C7_sz		-MMMbunnhummmmmmmmmmmmmhhhh	7619.5
GER_D1_sz		- MMM mmmmmmmmmmmmmmmmmmmmmmmmmmmmmmmmm	8230.3
GER_D2_sz		- MMM www.mmm.mmm.mmm.mmm.mmm.mmm.mmm.mmm.mmm	8704.8
GER_D3_sz		- MMMmmmmmmmmmmmmmmmmmmmmmmmmmmmmmmmmmm	8398.5
GER_D4_sz		- MM Marken Ma	7701.4
GER_D5_sz			7103.7
GER_D6_sz			
GER_D7_sz			
GER_D8_sz		-MMM.mmmmmmmmmmmmmmmmmmmmmmmmmmmmmmmmmm	
GER_D9_sz			
G032		-MMM manner manner	7565.7
G032		-MMM my more many many many many many many many many	
	04.00	04.20 04.40	.0000.
GERESS	1990-297:15.03.43.725	25/10/90 03:43:4	15 NORSAR

Fig. 7.2.3. Automatically generated teleseismic phase plot for GERESS, corresponding to the P-wave detection of the Novaya Zemlya explosion on 24 October 1990. The traces shown are a selection of single instruments filtered in the band 1.5–3.5 Hz. The bottom two traces are the P-beam filtered and unfiltered, using the velocity and azimuth determined by broadband FK analysis. The time window is 60 seconds.

EKY 1300 ha	am CO31 At 1990-29715 07 13 225 ppr 16 0	
Phase P vel	am G031 At 1990–297:15.07.13.225 snr 16.0 41.50 azi 17.70 rpw 0.560 q 1 a 3792.1 f 1.97 fband 1.50 3.50	
	┧╷╴╷╴╷╷╷╷╷╷╴╷╴╷╴╷╴╷╴╷╴╷╴╎╴╷ <mark>┤</mark> ┣╶╷╴╷╴╿╴╷╴╷╴╷╴╷╴╷╴╷╶╷╶┤╶╷┤	
GER_A0_sz	- Marken Ma	4391.7
GER_C4_sz		3451.5
GER_C5_sz	-www.mar.www.mar.www.mar.www.www.www.www.www.www.	
GER_C6_sz	fine warman warman for the second for the second se	
GER_C7_sz	f. www.www.www.www.www.www.www.www.www.w	
GER_D1_sz	-manus manus manus Manus manus manus	4007.0
GER_D2_sz	for the second s	3786.5
GER_D3_sz	-www.www.www.www.www.www.www.www.www.ww	4176.5
GER_D4_sz		3962.9
GER_D5_sz		2531.6
GER_D6_sz	-MW-MWMMMMMMMMMMMMMMMMMMMMMMMMMMMMMMMM	3062.3
GER_D7_sz		3905.6
GER_D8_sz		5626.4
GER_D9_sz		4004.3
G031		3792.1
G031	07.00 07.20 07.40	6059.8
GERESS	<u>1990–297:15.06.43.225</u> <u>25/10/90 03:52:</u>	33 NORSAR
<u></u>		a nononn

Fig. 7.2.4. Similar to Fig. 7.2.3, but showing the automatic plot for the PcP phase of the Novaya Zemlya explosion. Note the clear onset and the significant noise suppression on the filtered beam (second trace from bottom). Also note that the high estimated phase velocity (41.50 km/s) is a clear indication that this is indeed a core phase.

7.3 Generalized beamforming using a network of four regional arrays

The generalized beamforming method (GBF) for automatic phase association and event location (Ringdal and Kværna, 1989) has now been implemented for processing of data from the four regional arrays, ARCESS, FINESA, GERESS and NORESS. This method works from a list of phase detections for each array. For a large set of hypothetical event locations, GBF searches for a pattern of detections that fit the theoretically expected phase arrivals from the hypothetical locations. When a group of matching detections is found, the event location having the best fit to the data is chosen as the most likely epicenter.

In the following we present a brief report on our initial experience from applying GFB experimentally to the four-array network during a continuous five-day period.

Data analysis

A total of 600 beam grid points with an average separation of 150 km is used to span the geographical area of interest (see Fig. 7.3.1). This grid represents the initial (coarse) set of test locations, and whenever a match is found, a beampacking algorithm with a much denser grid is applied to refine the locations.

The GBF output from a typical 12-hour period is given in Table 7.3.1. For each associated event, the table lists the individual phase detections that either have defined the event or been associated as coda phases (p or s). Phase attributes (SNR, apparent velocity, dominant frequency, etc.) are also listed for each entry.

From Table 7.3.1 we find that the majority of the events are observed by one array only, whereas larger events have phase observations at two or more arrays. This is consistent with earlier studies of two-array and three-array networks.

It is interesting to notice that the incorporation of data from GERESS enables us to obtain more reliable event locations for events in northern Europe, as seen for the event in Poland with origin time 292:21.57.40 and epicenter location 51.70°N, 15.68°E. This event is presumed to be a rockburst in the Lubin mining area, and the location estimate is very close to that site.

In order to evaluate the performance of the method, we have analyzed GBF results from five consecutive working days (10/22/90 - 10/26/90). The results can be summarized as follows:

- 1. Several hundred regional events were associated, where the large majority were detected by one array only.
- 2. A total of 37 events had four or more associated phase detections, and the corresponding locations are shown in Fig. 7.3.2. After inspection we found that all but one of these events were properly associated and located. From Fig. 7.3.2 we see that the large majority of these events are located in the active mining areas of western USSR. We also notice a precise location of a nuclear explosion at Novaya Zemlya.
- 3. The occurrence of incorrect phase associations increases when we allow fewer than four phases to define an event.

Future work

From inspecting phase attributes, the analyst can in many cases identify erroneous phase associations based on inconsistencies among parameters like epicentral distance, apparent velocity and dominant frequency. Our next step will be to compile statistics on such attributes and make this kind of information available to the GBF program for use in the automatic computations.

We have also found that there is a need to refine the travel time models and also to improve the estimation of onset time for the different phase detections. Thereby, the automatic event locations will become even more precise.

Dynamic consistency checks using thresholds computed by the threshold monitoring method are also expected to help in identifying and removing unlikely phase associations. This will be particularly important at the time when detection data from the two three-component systems in Poland will be incorporated into GBF.

T. Kværna

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Ringdal, F. and T. Kværna (1989): A multichannel processing approach to real time network detection, phase association and threshold monitoring, *Bull. Seism. Soc. Am.*, 79, 1927–1940.

Origin time 1990-292:12.00.03.0 Lon 27.26 Timres 2.71 Wres 3.63 Nphase 3 Lat 59.80 Azres 3.65 Ph Pn Sn Pn Tres -0.6 7.1 0.3 Ares -5.0 2.2 -3.8 Arid 115935 115936 115940 Azim 55.1 ?kq 3 3 3 FIN FIN NRS AZ 160.1 160.1 90.0 Time 12.00.33.3 12.01.07.3 12.01.57.9 6.4 4.4 10.7 Snr 18.4 19.6 5.3 Amp 752.9 1474.2 237.0 Freq 6.07 3.45 3.59 .1 .3 .2 -2 Origin time 1990-292:12.04.36.0 Lat 50.50 Lon 12.11 Azres 0.58 Timres 0.43 Wres 0.58 Nphase 2 Dist 217.0 217.0 217.0 217.0 Az 328.6 328.6 328.6 328.6 328.6 Ph Pn P s Lg Time 12.05.09.5 12.05.17.1 12.05.30.5 12.05.37.0 Azim 327.6 335.9 330.1 328.5 Vel 7.4 7.9 3.3 3.9 Arid 181 182 183 184 Sta GER GER GER GER Ares -1.0 7.3 1.5 -0.1 Snr 13.2 4.5 12.3 3.8 Tres -0.6 Amp 4020.5 831.1 2018.7 1857.8 Freq 9.03 2.69 1.25 2.28 Fkq Pol 3212 -2 0.2 Nphase 3 Origin time 1990-292:12.06.12.0 Azres 3.52 Timres 0.32 Wres 1.20 Lat 59.50 Lon 24.04 Time 12.06.48.9 12.07.20.2 12.09.29.8 12.09.32.7 Dist 244.1 244.1 708.0 708.0 Az 208.2 208.2 95.7 95.7 Ph Pn Lg Lg s Vel 7.1 4.1 4.3 3.7 Sta FIN FIN Tres -0.6 -0.1 -0.2 Az1m Ares Snr Arid 203.1 206.2 99.1 -5.1 -2.0 3.4 0.3 28.7 17.0 3.6 2.7 754.8 1227.7 1032.6 834.6 5.48 3.23 1.50 2.12 -1 -2 -3 115939 115941 115946 3 3 1 2 NRS 99 96 . ō Lat 59.20 Timres 0.35 Wres 1.07 Nphase 2 Origin time 1990-292:12.08.49.0 Lon 27.52 Azres 2.89 Ph Pn Lg Tres 0.0 0.7 Ares -3.9 -1.9 Vel 7.3 3.8 Arid 115948 115949 Sta FIN FIN Snr 6.1 4.7 Fkq 3 3 Time Azim Freq 9.90 7.40 Dist Amp 306.5 708.1 Pol 161.7 161.7 12.09.28.8 12.10.03.1 262.6 157.8 Timres 1.11 Origin time 1990-292:12.28.03.0 Lon 32.68 Azres 2.05 Wres 1.63 Nphase 3 Lat 67.60 Dist 363.9 363.9 363.9 363.9 363.9 Time 12.28.56.4 12.29.04.5 12.29.35.2 12.29.44.3 12.29.47.5 Azim 121.8 125.5 118.3 122.8 125.3 Sta ARC ARC ARC ARC ARC Az 123.0 123.0 123.0 123.0 123.0 123.0 Ares -1.2 2.5 -4.7 -0.2 2.3 Vel 8.0 7.1 3.7 3.2 4.3 Snr 90.0 9.6 2.5 3.8 3.6 Fkq Pol 2 3 2 2 -2 2 Arid 115970 115971 115973 115974 Freq 4.73 6.38 4.72 3.25 4.44 Ph Pn P Sn Lg s Tres 1.1 Amp 3292.0 1945.9 1338.2 2015.0 3113.7 -1.8 -0.4 Origin time 1990-292:12.28.38.0 Azres 1.97 Timres 3.22 Wres 3.72 Lat 50.20 Lon 14.30 Nphase 3 Dist 156.8 156.8 1186.2 Tres 1.0 -8.7 0.1 Azim 16.6 12.3 172.0 173.7 Ares 0.9 -3.4 1.6 3.3 Vel 7.5 3.1 4.3 3.9 Az 15.7 15.7 170.4 170.4 Ariđ 187 188 Sta GER Ph Pg Rg Sn S Fkg Pol Amp 2374.7 650.6 409.1 12.29.04.3 12.29.22.5 12.33.08.1 4.6 22.7 2.5 11.9 9.98 1.01 4.49 GER 3 NRS 115982 NRS 115985 Nphase 3 Origin time 1990-292:12.30.18.0 Timres 4.50 Wres 6.72 Lat 50.80 Lon 12.59 Azres 8.90 Dist 231.8 231.8 1108.7 Ph Pn Lg Pn Tres 1.6 -11.8 -0.1 Vel 6.3 3.0 6.7 Snr 7.7 8.6 5.3 Azim 325.8 330.2 173.8 Freq 8.32 1.60 4.13 Fkq Pol Time Ares Amp 3574.5 1874.4 280.3 Arid 12.30.55.6 12.31.11.1 12.32.40.9 340.2 340.2 176.2 -14.4 -10.0 -2.4 190 192 115978 GER 3 1 3 GER -3

Table 7.3.1. GBF output from a typical 12-hour period. For each associated event, the table lists the individual phase detections that either have defined the event (Pn, Sn, Lg, Rg) or been associated as coda phases (p or s). Phase attributes (SNR, apparent velocity, dominant frequency, etc.) are also listed for each entry. (Page 1 of 3)

Origin time 1990-292:12.31.08.0	Lat Lon 56.20 26.39	Azres Timres Wres 11.07 3.89 6.66	Nphase 4	
Sta Dist Az FIN 584.9 178.1	Ph Time Pn 12.32.28.5	Tres Azim Ares	Vel Snr Amp	Freq Fkq Pol Arid
FIN 584.9 178.1	Pn 12.32.28.5 p 12.32.56.1	1.2 155.4 -22.7 185.0 6.9	9.4 4.5 77.3 7.1 32.1 1286.9	4.56 3 115980 3.91 1 115984
FIN 584.9 178.1 NRS 1000.7 113.8	Sn 12.33.24.0	-6.4 180.3 2.2	4.5 8.7 767.9	2.38 1 -2 115986
NRS 1000.7 113.8 GER 1185.3 41.6	Lg 12.35.55.0 Pn 12.33.39.4	7.1 99.4 -14.4 -0.9 46.6 5.0	3.4 2.7 660.2 6.2 9.1 143.9	2.35 2 115991 4.49 4 193
Origin time 1990-292:12.31.45.0	Lat Lon 67.60 33.47	Azres Timres Wres 2.34 1.17 1.75	Nphase 4	
Sta Dist Az ARC 390.1 119.8	Ph Time Pn 12.32.40.0	Tres Azim Ares -0.5 122.5 2.7	Vel Spr Amp 7.6 202.2 18647.9	Freq Fkq Pol Arid 6.78 l 115977
ARC 390.1 119.8	p 12.32.40.0	121.6 1.8	8.5 4.2 1185.3	6.78 1 115977 3.09 3 115979
ARC 390.1 119.8 ARC 390.1 119.8	p 12.32.50.5	117.8 -2.0	7.4 2.8 1568.1	8.43 4 115983
ARC 390.1 119.8 ARC 390.1 119.8	Sn 12.33.21.4 Lg 12.33.34.6	-3.2 124.8 5.0 0.4 118.2 -1.6	4.5 6.9 5042.9 3.2 7.8 11233.4	2.92 2 -1 115987 2.86 2 115990
ARC 390.1 119.8	s 12.33.39.0	120.4 0.6	4.8 5.4 10591.9	3.67 2 115994
NRS 1302.7 44.8	Pn 12.34.32.1	0.5 44.7 -0.1	8.4 4.0 265.2	3.35 3 115988
Origin time 1990-292:12.35.44.0	Lat Lon 61.00 29.03	Azres Timres Wres 4.27 2.23 3.29	Nphase 8	
Sta Dist Az	Ph Time	Tres Azim Ares	Vel Snr Amp	
FIN 166.4 106.0	Pn 12.36.09.8	-1.1 117.9 11.9	Vel Snr Amp 6.6 29.3 3083,2	Freq Fkq Pol Arid 6.99 3 -1 115989
FIN 166.4 106.0	Lg 12.36.29.2	-1.3 102.0 -4.0	4.0 25.2 1883.8	1.85 1 -2 115992
FIN 166.4 106.0 NRS 948.8 80.6	Rg 12.36.37.7 Pn 12.37.46.5	-2.7 111.3 5.3 -1.0 83.3 2.7	3.4 10.9 4734.5 11.4 8.9 730.2	1.24 1 115993 6.35 2 115995
NRS 948.8 80.6	Lg 12.40.07.4	-2.0 80.5 -0.1	4.6 2.6 835.6	1.36 2 115997
NRS 948.8 80.6 ARC 966.4 168.6	s 12.40.12.6 Pn 12.37.51.7	77.5 -3.1 2.0 169.2 0.6	4.1 3.9 1353.3 9.1 9.9 466.4	1.90 1 116001 5.42 2 115998
ARC 966.4 168.6	Sn 12.39.27.9	1.2 162.5 -6.1	4.7 3.0 402.9	5.42 2 115998 4.30 2 116000
ARC 966.4 168.6	Lg 12,40.07.8	-6.5 172.0 3.4	3.5 2.8 695.1	2.41 2 -3 116002
Origin time 1990-292:13.18.05.0	Lat Lon 59.50 27.89	Azres Timres Wres 5 0.83 0.19 0.39	Nphase 2	
Sta Dist Az	Ph Time	Tres Azim Ares	Vel Snr Amp	Freq Fkq Pol Arid
FIN 237.7 155.0 FIN 237.7 155.0	Pn 13.18.41.7 Sn 13.19.12.4	0.0 154.4 -0.6 0.3 153.9 -1.1	6.8 7.1 204.3 3.8 5.0 563.3	8.91 3 116032 7.06 3 -2 116033
114 13717 13310	54 13.17.14.4	0.5 155.5 1.1	5.0 5.0 505.5	7.00 3 -2 118033
Origin time 1990-292:13.36.54.0		Azres Timres Wres 7.98 0.66 2.66	Nphase 3	
Sta Dist Az FIN 227.4 198.1	Ph Time Pn 13.37.30.0	Tres Azim Ares 0.6 191.0 -7.1	Vel Snr Amp 7.8 16.5 392.4	Freq Fkg Pol Arid
FIN 227.4 198.1	Lg 13,37.56.3	-1.4 193.0 -5.1	4.0 23.2 1195.6	3.37 1 116045 2.83 1 -2 116046
NRS 750.8 94,7	Lg 13.40.24.1	0.0 83.1 -11.6	4.1 2.5 533.1	2.58 2 116050
Origin time 1990-292:13.49.09.0	Lat Lon 60.40 29.68	Azres Timres Wres 3 1.23 0.47 0.77	Nphase 2	
Sta Dist Az	Ph Time		¥a) 0	
FIN 227.6 119.2	Pn 13.49.44.1	Tres Azim Ares -0.4 118.6 -0.6	Vel Snr Amp 7.1 6.6 460.8	Freq Fkq Pol Arid 9.05 3 1 116071
FIN 227.6 119.2	s 13.50.06.4	121.2 2.0	4.1 5.8 769.0	5.57 3 -3 116073
FIN 227.6 119.2	Lg 13.50.12.1	-0.6 117.3 -1.9	3.1 3.9 444.4	1.14 1 -3 116074
Origin time 1990-292:14.24.30.0	Lat Lon 57.40 6.13	Azres Timres Wres 10.65 1.13 3.79	Nphase 3	
Sta Dist Az	Ph Time	Tres Azim Ares	Vel Snr Amp	Fred Fkd Pol And
NRS 484.2 222.2	Pn 14.25.36.3	-0.8 211.3 -10.9	9.0 10.8 635.0	Freq Fkq Pol Arid 8.20 1 1 116090
NRS 484.2 222.2 NRS 484.2 222.2	Lg 14.26.44.9	-0.5 224.7 2.5	4.0 3.6 909.2	2.13 1 116092
NRS 484.2 222.2 GER 1077.6 334.9	s 14.26.47.9 Sn 14.28.39.2	221.6 -0.6 2.1 353.5 18.6	4.1 3.2 954.8 4.0 3.6 175.5	2.56 1 116093 1.54 4 1 218
			1,010	
Origin time 1990-292:14.33.35.0	Lat Lon 48.40 30.42	Azres Timres Wres 2 5.87 0.22 1.69	Nphase 2	
Sta Dist Az	Ph Time	Tres Azim Ares	Vel Snr Amp	Freq Fkq Pol Arid
FIN 1478.5 167.3 NRS 1825.2 130.3	Pn 14.36.43.0 Pn 14.37.24.7	0.0 155.6 -11.7 -0.4 130.3 0.0	8.4 6.5 94.6	4.32 3 116095
MV2 1052'5 130'3	FU 14,3/,44,/	-0.4 I30.3 0.0	10.1 5.8 197.2	4.71 3 116096

Table 7.3.1. (Page 2 of 3)

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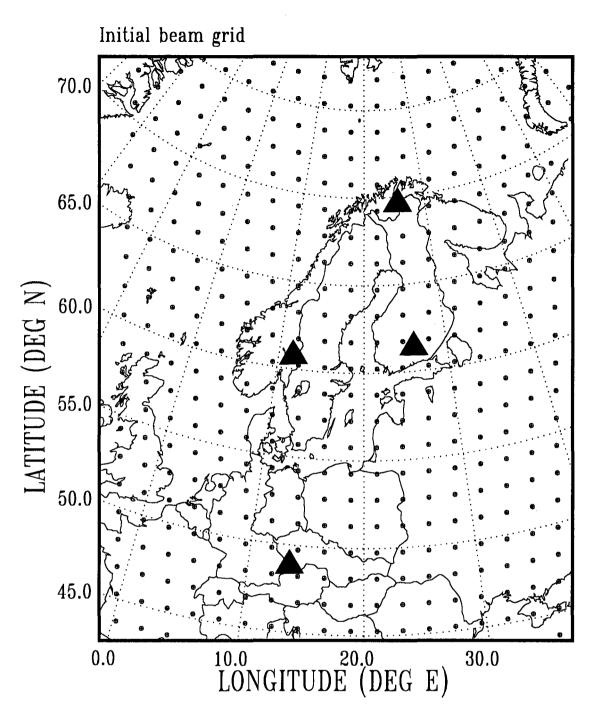
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Nphase 2 Wres 1.41 Origin time 1990-292:14.44.52.0 Lon 37.82 Azres 4.45 Timres 0.29 Lat 64.60 Ph Pn Sn Vel 8.3 4.2 Freq 8.81 8.16 Arid 116109 116111 Sta Dist Time Tres Azim Ares Amp 131.2 285.2 Fkq Pol Snr ARC 766.1 130.0 130.0 14.46.32.8 0.5 131.8 1.8 5.5 3 1 Nphase 2 Origin time 1990-292:14.56.29.0 Lon 12.11 Azres 4.25 Timres 0.48 Wres 1.54 Lat 49.90 Ph Pn Lg Vel 6.9 4.2 Arid 221 222 Sta Dist 164.9 164.9 Az 316.0 316.0 Time 14.56.55.2 14.57.15.7 Tres -0.4 0.6 Azim 310.5 319.0 Ares -5.5 3.0 Snr 3.0 7.2 Freq 7.64 4.18 Fkq Pol 3 3 -2 Amp 1375.0 1416.7 GER Nphase 2 Origin time 1990-292:15.59.44.0 Lat 59.20 Lon 11.31 Azres 2.60 Timres 0.52 Wres 1.17 Dist 171.7 171.7 Ph Pn Sn Azim 185.3 180.1 Az 184.5 184.5 Time Tres 0.2 -0.8 Ares 0.8 -4.4 Vel 7.0 3.9 Snr 13.6 4.7 Freq 4.38 9.00 Fkq Pol 1 3 -3 Arid 116126 116127 Sta Amp 462.6 864.1 NRS NRS 16.00.11.8 16.00.34.5 -- 3 Origin time 1990-292:16.09.58.0 Lon 11.64 Timres 0.29 Wres 1.68 Nphase 2 Lat 49.60 Azres 5.55 Ph Pn Lg Time 16.10.25.2 16.10.46.0 Sta GER GER Dist 171.9 171.9 Az 300.0 300.0 Tres -0.5 -0.1 Azim 289.5 300.6 Ares -10.5 0.6 Vel 6.5 4.0 Snr 4.0 3.3 Amp 800.7 758.0 Freq 9.71 4.95 Fkq Pol Arid 4 228 229 Nphase 2 Origin time 1990-292:20.46.18.0 Timres 0.43 Wres 1.78 Lat 60.70 Lon 21.82 Azres 5.40 Dist Az Ph 244.7 252.1 Pn 244.7 252.1 Sn Time 20.46.55.3 20.47.27.1 Tres -0.3 0.5 Vel 8.7 4.6 Azim 261.7 253.2 Ares 9.6 1.1 Snr 5.7 3.8 Sta FIN FIN Amp 115.6 241.1 Freq 4.22 4.66 Fkq Pol 2 3 -3 Arid 116244 116245 Origin time 1990-292:21.57.40.0 Lon 15.68 Azres 4.23 Timres 1.70 Wres 2.75 Nphase 6 Lat 51.70 Time 21.58.30.3 21.58.43.8 21.59.25.2 21.59.38.5 21.59.54.8 22.00.04.8 22.00.38.5 22.00.21.3 22.02.26.0 Az 23.2 23.2 23.2 23.2 23.2 163.9 163.9 163.9 215.0 Amp 2858.7 3017.5 4004.7 8589.2 4114.4 383.9 245.6 417.7 195.6 202.5 Azim 29.3 25.0 25.6 26.2 29.8 166.3 162.3 167.9 217.4 207.5 Dist Vel 8.9 6.4 6.3 4.2 5.3 8.3 9.7 4.8 9.8 4.9 Ph Pn P Lg S Pn Sta Tres 0.0 Ares Snr Freq 2.75 2.64 2.49 2.27 1.00 3.42 4.02 2.27 3.78 2.84 Fkg Pol Arid Dist 347.5 347.5 347.5 347.5 347.5 1038.4 1038.4 1038.4 1256.7 1256.7 Arid 253 254 255 257 258 116282 116283 6.1 1.8 2.4 3.0 6.6 2.4 -1.6 4.0 2.4 -7.5 64.9 17.3 8.7 3.4 3.2 17.1 4.5 3.7 23.8 GER 1 1 1 1 GER GER GER GER NRS 3 1 1 1 1 1 2 1 8,0 3 0.4 p Sn Pn Sn NRS NRS -0.4 0.3 1.1 116284 FIN 1 116281 FIN 1256.7 215.0 2.6 116286 Timres 2.29 Nphase 5 Lat 67.90 Lon 19.99 Wres 4.09 Origin time 1990-292:23.36.38.0 Azres 7.23 Time 23.37.20.6 23.37.25.5 23.37.46.9 23.37.53.4 23.38.03.4 23.40.11.7 23.38.34.8 Azim 225.4 221.6 221.7 227.8 225.3 346.2 32.3 Ares -8.0 -11.8 -11.7 -5.6 -8.1 5.5 9.0 Freq 6.11 4.11 3.67 3.61 1.42 1.79 3.45 Fkq Pol 2 -1 2 1 2 1 1 3 Snr 55.2 7.3 2.4 15.2 3.0 3.0 5.4 Amp 1175.6 695.8 762.6 2346.3 2834.8 198.6 Arid 116311 116312 116313 116314 116315 Ph Pn P Sn Lg Lg Pn Tres -0.4 Sta Dist Vel 7.4 6.7 7.1 5.0 4.0 4.1 8.3 AZ Dist 288.7 288.7 288.7 288.7 288.7 288.7 776.3 896.3 AZ 233.4 233.4 233.4 233.4 233.4 233.4 340.7 23.3 ARC ARC ARC ARC ARC FIN -2.5 4.7 -3.4 -0.4 116310 NRS 114.1 116309 Nphase 3 Origin time 1990-292:23.42.32.0 Lon 20.04 Azres 1.54 Timres 2.52 Wres 2.90 Lat 67.30 Time 23.43.21.2 23.43.23.5 23.43.32.7 23.43.53.8 23.44.06.9 Dist 335.7 335.7 335.7 335.7 335.7 Az 224.6 224.6 224.6 224.6 224.6 Azim 225.2 220.3 226.8 225.5 221.5 Fkq Pol 1 -1 2 3 2 1 Ares 0.6 -4.3 2.2 0.9 -3.1 Vel 7.5 7.3 7.4 4.8 4.3 Amp 979.0 470.3 443.2 944.5 Freq 6.33 5.04 3.99 4.68 2.90 Arid 116316 116317 116318 116319 116320 Sta Ph Pn P Sn Lq Tres 0.4 Snr 5nr 24.7 6.1 4.8 6.3 4.8 ARC ARC ARC ARC ARC -6.2 1.0 1896.3

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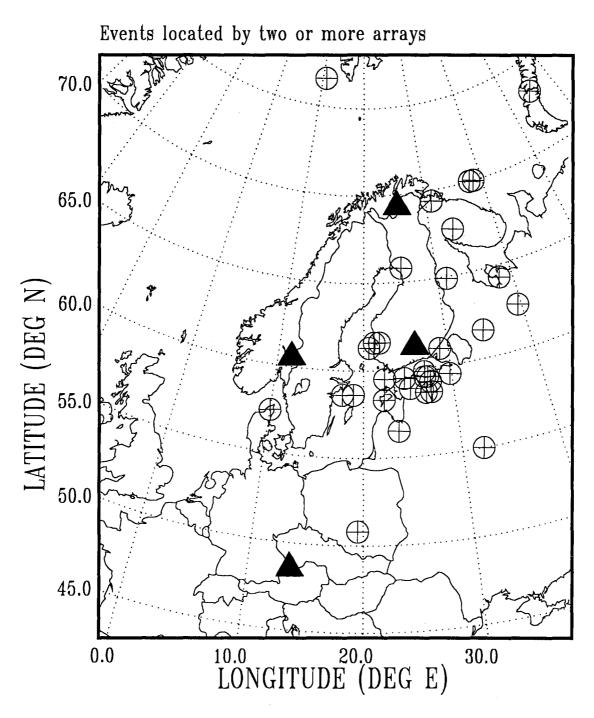
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Map projection: LAMBERT EQUAL AREA, AZIMUTHAL

Fig. 7.3.1. Initial beam grid used by the generalized beamforming method when processing data from four regional arrays. ARCESS, FINESA, NORESS and GERESS are marked with solid triangles.



Map projection: LAMBERT EQUAL AREA, AZIMUTHAL

Fig. 7.3.2. Events located by GBF having four or more associated phase detections. The data cover the five-day period 22-26 October 1990. Out of a total of 37 events, 12 were located by two arrays, 22 by three arrays and 3 by four arrays. The four regional arrays, ARCESS, FINESA, NORESS and GERESS, are marked with solid triangles.

7.4 Continuous threshold monitoring of the Novaya Zemlya test site

Introduction

The continuous threshold monitoring technique (Ringdal and Kværna, 1989) represents a new approach toward achieving reliable seismic monitoring for the purpose of verifying nuclear test ban treaties.

Traditionally, seismic monitoring has relied upon applying signal detectors to individual stations within a monitoring network, associating detected phases and locating possible events in the region of interest. This procedure has been accompanied by assessments of network capabilities for the target region, usually by applying statistical models for the noise level distribution, introducing station corrections for signal attenuation and devising a combinational procedure to determine the detection threshold as a function of the number of phase detections required for reliable location.

The statistical noise models used in these capability assessments are not able to accommodate the effect of interfering signals, such as the coda of large earthquakes, which may cause the estimated thresholds to be quite unrealistic at times. Furthermore, only a statistical capability assessment is achieved, and no indication is given as to particular time intervals when the possibility of undetected clandestine explosions is particularly high.

The continuous threshold monitoring technique alleviates all of these problems. It makes it possible to ascertain, at any point in time, for a given target region, the maximum magnitude of a possible clandestine explosion at a predefined level of confidence. This makes it possible to focus attention upon those specific time intervals when realistic evasion opportunities exist, while retaining confidence that no treaty violation has occurred at other times.

Application to the Novaya Zemlya test site

In order to demonstrate how such monitoring could be performed in a practical operational situation, we have conducted an experiment during which we have applied continuous threshold monitoring to the Novaya Zemlya test site for a full one-week period. Our data base has been the Fennoscandian regional array network (NORESS, ARCESS, FINESA). As illustrated in Fig. 7.4.1, these three arrays are all within regional distances from the test site, with excellent P-phase detection capabilities (Fig. 7.4.2). The ARCESS array also detects S phases from Novaya Zemlya explosions quite well, whereas NORESS and FINESA have a lower S-phase detection capability.

The parameters used in the threshold monitoring experiment are given in Table 7.4.1. For each array, we steer "optimum" P and S beams towards the test site, and calibrate these beams using actually observed signal attenuation from Novaya Zemlya explosions. By focusing in this way on the target region, we can at any point in time measure the "noise magnitude" for a given phase at a given array, and combine these data to obtain a network threshold as explained in detail by Ringdal and Kværna (1989).

Results

Figs. 7.4.3-7.4.9 show the result of the monitoring experiment. Each of these figures covers one data day, starting 24 October 1990. The upper three traces of each figure represent the thresholds (i.e., 90 % upper magnitude limits) obtained from the three individual arrays, whereas the bottom trace illustrates the network threshold. Typically, the individual array traces have a number of significant peaks for each 24-hour period, due to interfering events (local or teleseismic). On the network trace, the number and sizes of these peaks are greatly reduced, because an interfering event will usually not provide matching signals at all the stations. From probabilistic considerations, it can in such cases be inferred that the actual network threshold is lower than these individual peaks might indicate.

On each of the one-day figures, we have included comments explaining the presence of the most significant peaks on the network trace. Here, we will just note that the first day, 24 October 1990, was the day of an actual nuclear explosion ($m_b = 5.7$) on Novaya Zemlya, and this event naturally stands out on the plot. While the peak value of the network threshold plot does not represent the actual magnitude of the event, it is in fact quite close (5.64).

As a general comment to Figs. 7.4.3–7.4.9, we note that such plots, which are easily generated by the Intelligent Monitoring System (IMS) (Bache *et al*, 1990), will enable the analyst to obtain an instant assessment of the actual threshold level of the monitoring network. The peaks on the network traces may be quickly correlated with the IMS detection bulletin, in order to decide whether they originate from interfering events or from events in the target region.

Discussion

In a monitoring situation, it will be important to isolate and analyze more extensively those time intervals which offer significant evasion opportunities. Table 7.4.2 gives a statistic of the number of occasions during which the upper magnitude limit exceeded a given level. In theory, if this limit is, e.g., at 3.0, it might be possible that a clandestine $m_b = 3.0$ explosion had occurred without being detected. There are many options available to investigate such a hypothesis in more detail, although we have not attempted to do so in this study. The most immediate approach would be to analyze high-frequency signals for the time interval being considered. For example, on ARCESS records Novaya Zemlya explosions will contain significant energy at 10 Hz and above, even at magnitudes well below 3.0. Teleseismic events, even of large m_b , will not contain much energy at these frequencies and thus it might be possible to obtain additional indications from these data.

To assess interfering phases from events at regional distances is more difficult, since the high-frequency energy might not discriminate such events from Novaya Zemlya explosions. In such cases, additional procedures, such as maximum likelihood beamforming, might become useful to suppress signals from the interfering event and thereby obtain a more realistic estimate of the signal energy arriving from the target region.

It is significant that the 3-array network studied in this paper can monitor the Novaya Zemlya test site down to m_b 2.5 or below more than 99 % of the time (Fig. 7.4.10). Further improvements would clearly be possible by adding more stations to the monitoring network, especially highly sensitive stations at other azimuths than those covered by the Fennoscandian network. This would in particular contribute to lowering the peaks due to interfering events, whereas any event truly originating in the target region would of course still stand out clearly on the combined network traces.

In conclusion, the continuous threshold monitoring has been demonstrated to provide a simple and very effective tool in day-to-day monitoring of a site of particular interest. Further research will focus upon developing methods to analyze time intervals during which significant evasion possibilities might exist. Data from the regional arrays, the large-aperture NORSAR arrray, as well as other available stations, will be used in these analyses.

T. Kværna F. Ringdal

References

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Station	Phase	Tr. Time	App. Vel.	Azim.	Filter	Config.	STA_len.	Tim. Tol.	Sta_Calib
ARC	Pn	148.0	9.9	60.5	3.0-5.0	A0,B,C,D	2.0	2.0	0.754
ARC	\mathbf{Sn}	257.0	4.9	53.2	3.0 - 5.0	A0,B,C,D	5.0	3.0	1.176
FIN	Р	228.0	9.6	32.9	2.0 - 4.0	А0,В,С,	2.0	2.0	1.520
NRS	Р	284.0	10.4	28.1	1.5 - 3.5	A0,B,C,D	2.0	2.0	0.677

Tr. time		Travel time of phase
App. vel.		Apparent velocity from broadband F-K measurement
Azim.	—	Azimuth from broadband F-K measurement
Filter		Cutoffs of bandpass filter (3rd order Butterworth)
Config.		Array configuration used in beamforming. A0,B,C means
		A0Z, B-ring and C-ring
STA_len.		STA length in seconds
Tim. tol.	—	Time tolerance when searching for maximum STA
STA_calib.	—	Calibration factor used when converting STA values
		(in quantum units) to magnitude.
		$Magnitude = log10(STA) + STA_calib.$

Table 7.4.1.

			Total					
	297	298	299	300	301	302	303	(one week)
$m_b \geq 4.0$	1	0	0	0	0	0	0	1
$\mathrm{m}_b \geq 3.5$	1	1	0	0	0	0	0	2
$m_b \geq 3.0$	3	2	2	0	0	0	0	7
$\mathrm{m}_b \geq 2.5$	5	12	5	0	3	6	3	34

Table 7.4.2. Statistics of peaks in the network threshold traces. See also comments on Figs. 7.4.3-7.4.9.

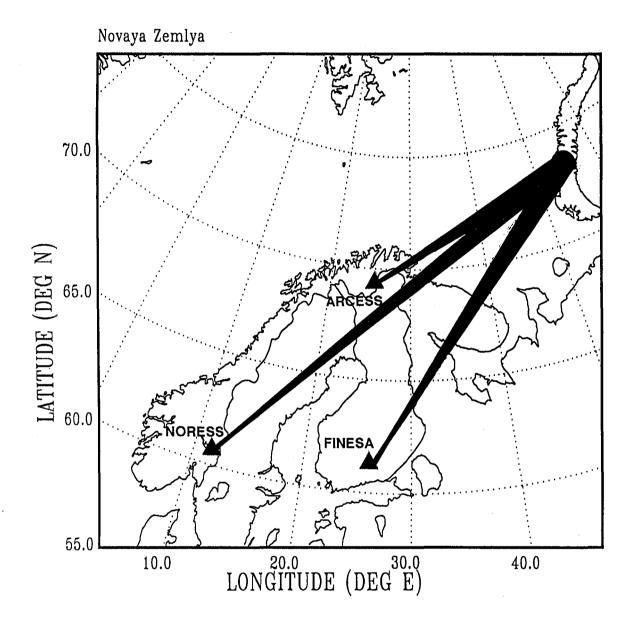
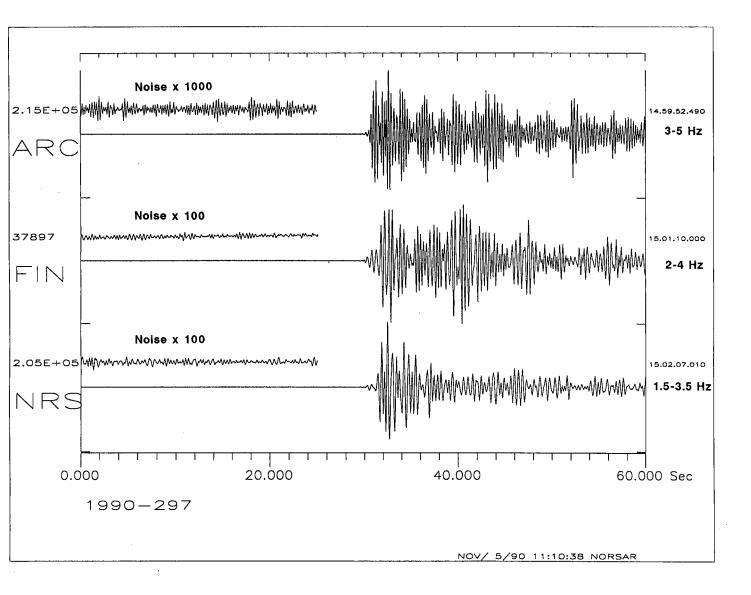
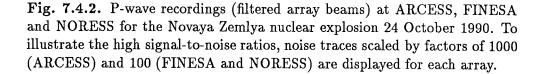
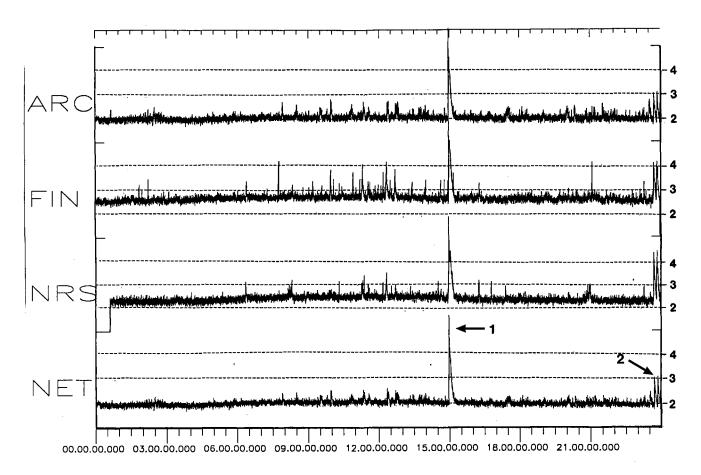


Fig. 7.4.1. Location of the target area (Novaya Zemlya) for the threshold monitoring experiment. The locations of the three arrays NORESS ($\Delta = 2280$ km), ARCESS ($\Delta = 1110$ km) and FINESA ($\Delta = 1780$ km) are indicated.







1990-297:00.00.00.000

Fig. 7.4.3. Threshold monitoring of the Novaya Zemlya test site for day 297 (24 October 1990). The top three traces represent thresholds (upper 90 per cent magnitude limits) obtained from each of the three arrays (ARCESS, FINESA, NORESS), whereas the bottom trace shows the combined network thresholds.

- 1. An underground nuclear explosion $(m_b = 5.7)$ at Novaya Zemlya at 14.58.00 GMT. The peak of the network trace is 5.64.
- 2. Two teleseismic earthquakes from N. Xinjang province, China $(m_b = 5.2 \text{ and } 5.4)$. The P-wave train from each of these earthquakes causes the network threshold to increase to about $m_b = 3.0$ for the target region.

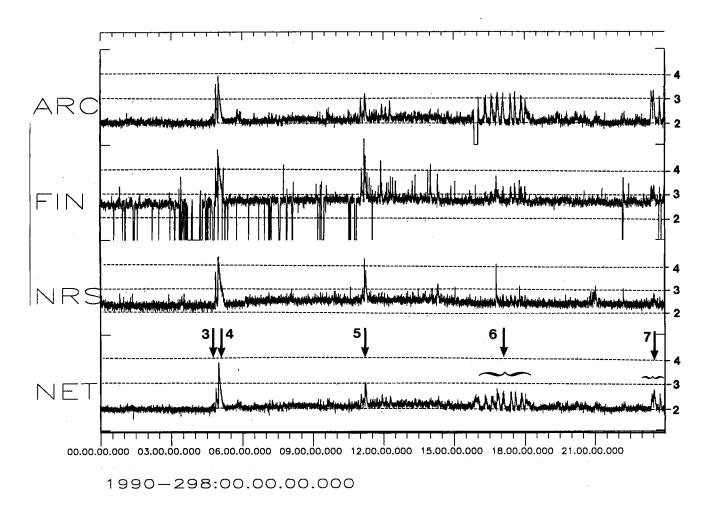
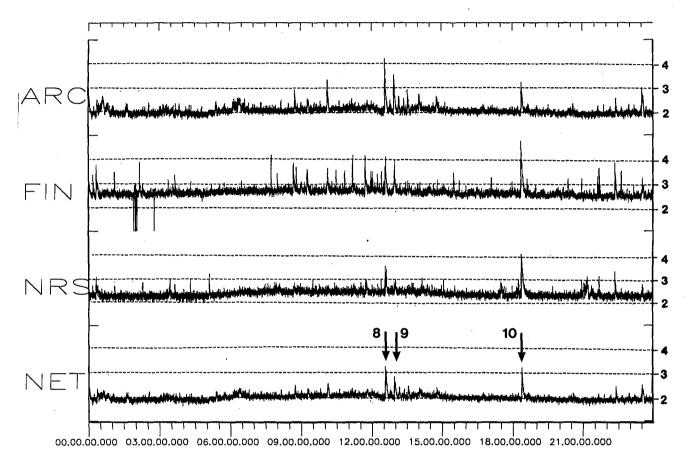


Fig. 7.4.4. Same as Fig. 7.4.3, but for day 298 (25 October 1990). The FINESA array had several short outages this day, but this caused no particular problems in terms of network threshold capacity.

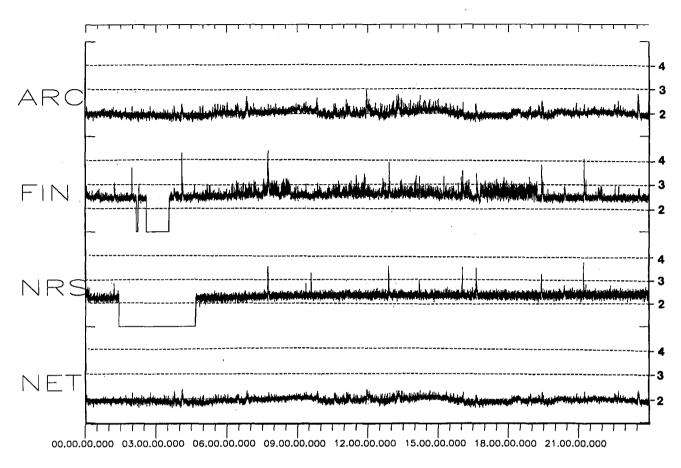
- 3. An earthquake $(m_b = 4.5)$ near Jan Mayen. The corresponding network threshold peak for Novaya Zemlya is $m_b=2.8$.
- 4. A teleseismic earthquake ($m_b = 6.0$) at Hindu Kush. The relatively strong P-wave train caused a peak threshold of $m_b = 3.8$ for monitoring Novaya Zemlya.
- 5. A teleseismic earthquake $(m_b = 5.9)$ at Mindanao, Philippine Islands. Corresponding threshold is $m_b = 3.0$.
- 6-7. A sequence of seismic events (presumably underwater explosions) near Murmansk, Kola Peninsula. The network threshold for monitoring Novaya Zemlya is about $m_b = 2.5$ to 2.8 at the times of these events.



1990-299:00.00.00.000

Fig. 7.4.5. Same as Fig. 7.4.3, but for day 299 (26 October 1990).

- 8. A large mining explosion $(M_L = 3.0)$ near the Norway-USSR border. The Novaya Zemlya threshold peak is $m_b = 3.2$. Note that this threshold exceeds the event magnitude; this is because of the proximity of the event to the network stations.
- 9. A large mining explosion $(M_L = 2.5)$ at the Kola Peninsula. The Novaya Zemlya threshold peak is $m_b = 2.8$.
- 10. A teleseismic earthquake $(m_b = 5.1)$ near Lake Baikal. The network threshold peak is $m_b = 3.2$.

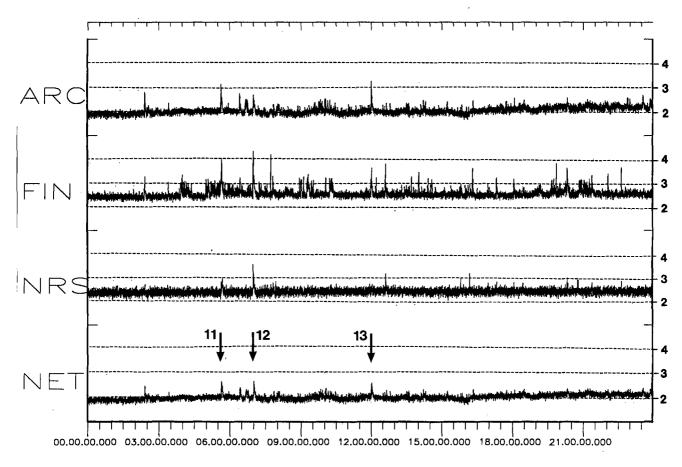


1990-300:00.00.00.000

Fig. 7.4.6. Same as Fig. 7.4.3, but for day 300 (27 October 1990).

Notes:

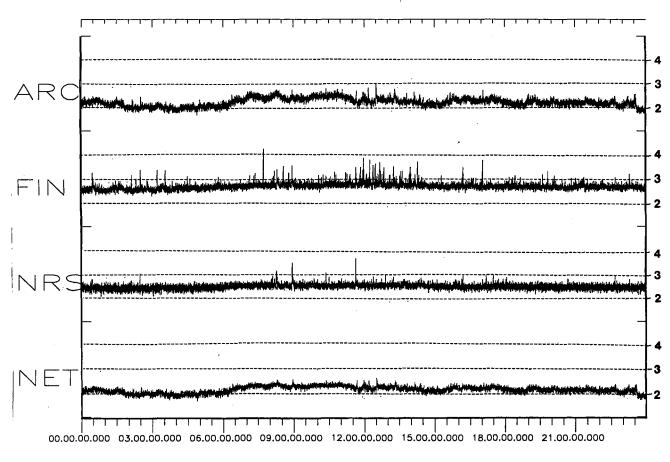
No significant peak during this day. The simultaneous outages at FINESA and NORESS did not cause significant problems for the network threshold monitoring.



1990-301:00.00.00.000

Fig. 7.4.7. Same as Fig. 7.4.3, but for day 301 (28 October 1990).

11 and 13.	Two large mining explosions $(M_L = 2.5)$ on the Kola
	Peninsula. Network threshold is about $m_b = 2.6$.
12.	A teleseismic earthquake $(m_b = 5.3)$ at the Kurile Islands
	Network threshold is $m_b = 2.7$.

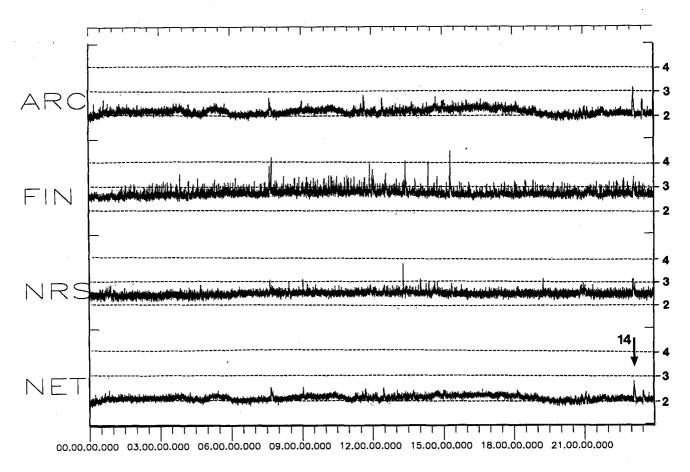


1990-302:00.00.00.000

Fig. 7.4.8. Same as Fig. 7.4.3, but for day 302 (29 October 1990).

Notes:

No significant peaks in the network threshold plot this day.



1990-303:00.00.00.000

Fig. 7.4.9. Same as Fig. 7.4.3, but for day 303 (30 October 1990).

Notes:

14. A small earthquake ($M_L = 2.8$) in Nordland, N. Norway, caused an increase in the network threshold for Novaya Zemlya to $m_b = 2.8$.

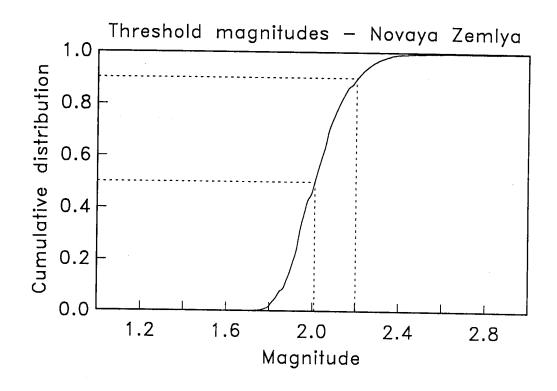


Fig. 7.4.10. Cumulative statistics of the network threshold magnitudes from Figs. 7.4.3-7.4.9, covering one full week of data.

7.5 Real-time processing using a hybrid 3-component / small array station

Introduction

In recent years, much effort has been devoted to developing and assessing various methods for 3-component seismic data processing. It has been demonstrated that polarization analysis can provide P azimuth estimates with good accuracy from a single 3-component station. Using SH or SV particle motion models, some success has also been reported in determining azimuth from S and Lg phases, although there is often a 90 or 180 degree ambiguity in the resulting estimates.

These efforts notwithstanding, a fundamental problem in automatic 3component processing still remains. This is the problem of phase identification, which of course is essential in deciding which particle motion model to apply. From our experience at NORESS, a high degree of rectilinearity, which in theory would indicate the presence of a P phase, is quite often seen also for S and Lg phases, and even for noise bursts, when applying polarization analysis. As a result, an automatic P-type solution found by 3-component processing is often of limited usefulness, since it may either be a P phase (with correct azimuth) or some other phase (in which case the azimuth estimate is useless).

Small-aperture arrays of the NORESS-type have proved to be very effective in processing regional as well as teleseismic phases. Their primary features are:

- Significant SNR gains at high frequencies
- Reliable phase identification (P-type versus S-type phases)
- Precise azimuth estimates of all phase types.

While the accuracy of NORESS azimuth estimates can be as good as \pm 1 degrees for well-calibrated regions, the uncertainty of uncalibrated azimuth estimates is often of the order of 10 degrees or more, due to lateral inhomogeneities near the receivers. In practical schemes for automatic phase association (e.g., Mykkeltveit and Bungum, 1984), a tolerance of 30 degrees in azimuth deviation from the true value is often assumed. Given that the acceptable limits in azimuth estimation for phase association purposes are much less restrictive than the optimum array capability, a natural question is whether a smaller regional array can achieve reliable phase identification as well as an acceptable uncertainty in azimuth estimation.

We have attempted to address this question, and have chosen to evaluate the smallest such array available to us: the NORESS A-ring subarray (Fig. 7.5.1). This subarray comprises a center 3-component seismometer A0, surrounded by a triangular SPZ array A1-3. The diameter of this subarray is only 0.3 km, i.e., a factor of 10 less than NORESS, and it thus spans an area only 1 per cent of that of the full NORESS array. In this paper, we present an initial evaluation of automatic detection processing using this very small array.

Automatic processing

We conducted automatic detection processing of the A-ring subarray for a period of 5 days (22-26 October 1990), using a standard multi-filter power detector with parameters as specified in Table 7.5.1. For each detected signal, broadband F-K analysis was conducted using the 4 SPZ sensors, and compared to the NORESS F-K results. We also carried out polarization analysis (using a P-wave particle motion model) for each detected phase, applying the method of Kværna and Doornbos (1986) to the 3-component A0 system.

To obtain a data base for the evaluation, we extracted all seismic phases detected by NORESS and associated to verified regional events for the 5-day period. The generalized beamforming procedure (Ringdal and Kværna, 1989) and the results from IMS processing (Bache *et al*, 1990) were used in order to ensure correct location of these reference events. P-coda detections and multiple S-phases were ignored, so that each event provided a maximum of 3 phases (P, S and Lg). These phases were then matched to the detection lists produced from the A-ring SPZ subarray and the 3-component analysis, and the phase velocity and azimuth estimates were compared.

Phase identification

Fig. 7.5.2 shows the A-ring phase velocity F-K estimates for P phases (circles) and S phases (crosses) for the reference data set. The separation is better than 95 per cent, which implies that even this small array is able to provide correct phase identification automatically and with high confidence. The corresponding picture for the full NORESS array is shown in Fig. 7.5.3, and naturally shows a better separation. It should be noted here that all the reference phases were by definition correctly identified by NORESS, so it is not surprising that the separation is 100 per cent. But it is still interesting to compare the scatter in the two data sets.

P-wave azimuths

Fig. 7.5.4 compares P-wave azimuths estimated by the full NORESS SPZ array and the small A-ring SPZ subarray using broadband F-K analysis in both cases. The estimates are very consistent, and the large majority are well within a tolerance limit of 30 degrees.

A corresponding plot for P waves analyzed from 3-component records is given in Fig. 7.5.5, and shows a similar amount of scatter. In fact, the scatter is slightly less than in Fig. 7.5.4. Thus, the polarization analysis can give very useful contributions to regional azimuth estimates, assuming that the phase first has been identified as a P phase. An interesting approach would be to combine the two azimuth estimates (A-ring SPZ and 3-comp) in order to obtain increased stability.

S-wave azimuths

Fig. 7.5.6 compares azimuths of S-type phases estimated by the A-ring SPZ subarray and the full NORESS array. Again, the correspondence is quite good, and thus shows that automatic regional phase association using RONAPP-type processing can be achieved even when using an array as small as 0.3 km in diameter. We note that our 3-component processing provides no useful azimuth information for S phases, but it is of course possible that such information could be obtained in certain cases, given that the phase first has been identified as S or Lg.

Detectability

Figs. 7.5.7 and 7.5.8 illustrate the P and S wave detectability of the Aring array as a function of NORESS SNR. From Fig. 7.5.7, it is seen that all P phases with SNR > 20 dB (i.e., STA/LTA > 10 at NORESS) have been detected. At distances below 500 km, several events of relatively low SNR at NORESS have also A-ring detections; this is due to the high signal frequencies which cause the full array SNR gains of these phases to be less than the theoretical \sqrt{N} . At distances above 500 km, the superiority of the full NORESS array becomes apparent.

In Fig. 7.5.8 it is seen that the A-ring subarray is close to matching NORESS S-phase detectability at all distances. This is because the horizontal components of the A0 3-component system provide quite efficient detection of S and Lg phases, in particular when added incoherently to the vertical component. The full array does not have the same SNR gain for secondary phases as for P-phases, because of less signal coherency and (in particular) coherent noise caused by P coda. Thus, as expected, there is not a significant difference in secondary phase detection.

False alarm consideration

In practical operation of any seismic system, the problem of false detections is very important. This is especially the case if the online detector is operated at a low detection threshold, and it is essential to be able to identify false alarms at as early a stage as possible.

To address this problem, we have analyzed in detail all the A-ring detections for one full data day (24 October 1990). The results are presented in Table 7.5.2, again with NORESS results as a reference. From the table, it is seen that out of 117 total phase detections, 105, or 90 per cent, were correctly classified using the broadband F-K analysis applied to A-ring SPZ data. Of these 105 phases, 37 were P, 36 S (or Lg) and 32 noise (i.e., low-velocity detections). Note that P coda detections were counted as P and S coda were counted as S in these statistics. None of the 37 phases which (according to NORESS) were of the P type were misclassified by the A-ring. Of the 40 S phases, 4 were misclassified (2 P and 2 noise). Out of 40 noise detections, 3 were given P-phase velocities and 5 were given S-phase velocities when using the A-ring.

These statistics must be considered quite satisfactory. In fact, it appears that the SNR threshold for the A-ring detector could be lowered significantly, and still produce a reasonable false alarm rate.

Conclusions

The problems encountered when using a 3-component system in a realtime automatic processing environment appear to be effectively alleviated by supplementing the 3-C system with a very small (aperture 0.3 km) 3-element array. Based on the studies in this paper of the NORESS A-ring subarray, we conclude that:

- Phase identification (P or S) can be reliably achieved (better than 95 % success rate) using F-K analysis of the A-ring array data.
- Azimuth estimates, with accuracy generally to within 30 degrees can be obtained for both P and S phases using A-ring array processing, and (at least) for P-phases using 3-component polarization analysis of the A0 3-component station..
- Good regional P-phase detectability can be obtained from the A-ring array out to 500 km epicentral distance. At greater distances, P-wave detectability relative to that of NORESS deteriorates sharply.
- Detectability of S-phases using the A-ring array is excellent at all distances, and comes close to matching that of the full NORESS array.
- The A-ring array analysis makes it possible to isolate the majority of noise detections, thus giving an acceptable false alarm rate for online operation.

It would be an interesting experiment to supplement some existing 3component stations with a triangular small array as described here, and conduct network detection and location experiments. Before doing so, it is of course important to verify that these results can be obtained in other geological and geographical environments, e.g., by analyzing similar data for other existing arrays (ARCESS, GERESS, FINESA). A very small array of the A-ring type is especially suited for processing high signal frequencies. In fact, one might consider a dense sensor deployment within the A-ring aperture, as an experiment aimed at conducting array processing at frequencies of 20-40 Hz. This would of course require a higher sampling rate than the 40 Hz currently used at NORESS. Array processing at these frequencies would be of particular interest in the context of developing methods for monitoring cavity decoupled explosions, which might have significant signal energy in this frequency band.

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Coherent beams:

Incoherent beams:

Beam	Apparent vel.	Azimut	Filter bar	nd Configuration	Threshold
NA01	9999.9	0.0	0.5 - 1.5		2.7
NA02	9999.9	0.0	1.0- 2.0	A0z,A0n,A0e	2.6
NA03	9999.9	0.0	1.0- 3.0	A0z,A0n,A0e	2.5
NA04	9999.9	0.0	1.5- 2.5	5 A0z,A0n,A0e	2.5
NA05	9999.9	0.0	1.5- 3.5	5 A0z, A0n, A0e	2.5
NAOG	9999.9	0.0	2.0- 3.0	A0z,A0n,A0e	2.6
NAO7	9999.9	0.0	2.0- 4.0	A0z,A0n,A0e	2.8
NA08	9999.9	0.0	2.5-4.5	5 A0z, A0n, A0e	3.4
NAO 9	9999.9	0.0	3.0- 5.0	A0z,A0n,A0e	3.5
NA10	9999.9	0.0	3.5- 5.5	5 A0z,A0n,A0e	2.8
NA11	9999.9	0.0	4.0- 8.0	A0z,A0n,A0e	2.5
NA12	9999.9	0.0	5.0-10.0	A0z,A0n,A0e	2.5
NA13	9999.9	0.0	8.0-16.0) A0z,A0n,A0e	2.8
				• •	

Table 7.5.1. Parameters used for the A-ring detector experiment.

	Classified as:			
Correct	P	S or Lg	Noise	
Phase id	(v>6 km/s)	(<u>3.4<v≤6 km="" s<="" u="">)</v≤6></u>	(v≤3.4 km/s)	
P	37	0	0	
S or Lg	2	36	2	
Noise	3	5	32	

Total phases detected by the A-ring detector : 117 Total phases correctly classified : 105 (90 %)

Table 7.5.2. Statistics of detected phases for the A-ring array for a 24-hour period. The phases are classified based on estimated phase velocities using A-ring SPZ broadband F-K, and the "correct" phase id is based on F-K results from the full NORESS array.

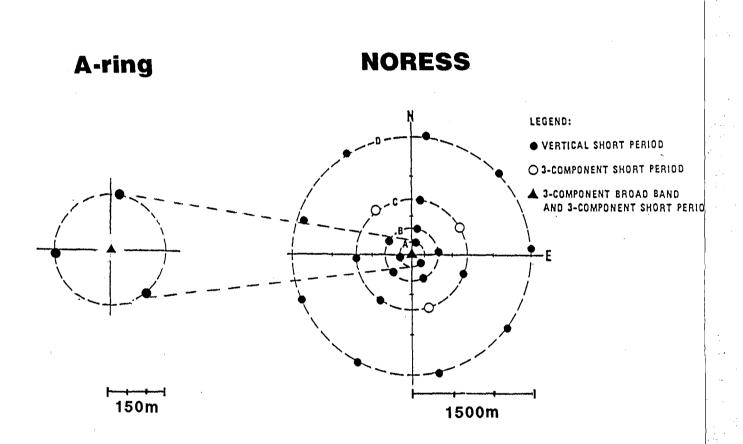


Fig. 7.5.1. Geometry of the full NORESS array and of the A-ring subarray used in this study.

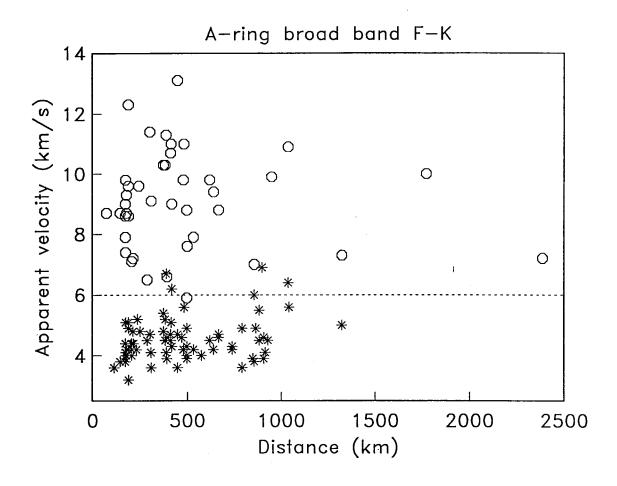


Fig. 7.5.2. Estimated phase velocities using the A-ring SPZ array (broadband F-K) for detected P phases (circles) and S phases (asterisks). Note that the phases can be identified from phase velocity with more than 95 % accuracy.

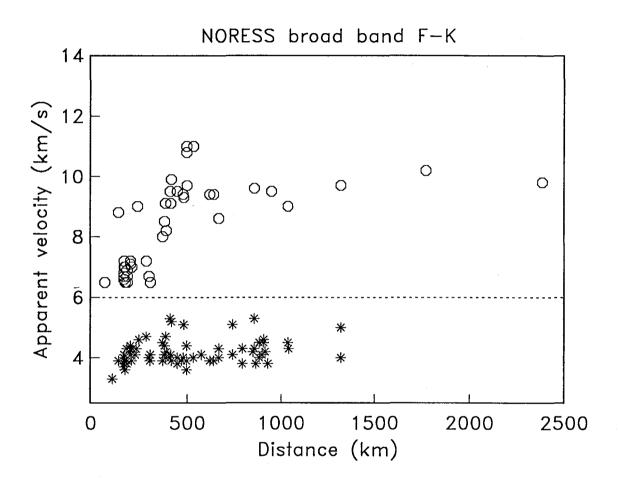


Fig. 7.5.3. Similar to Fig. 7.5.2, but with phase velocities estimated using the full NORESS array.

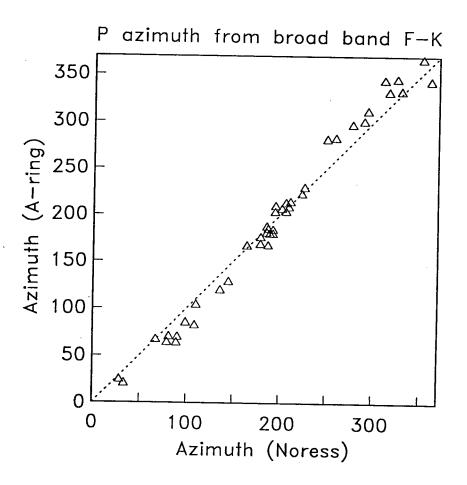


Fig. 7.5.4. Comparison of estimated azimuths of P phases using the full NORESS array and the A-ring SPZ array (broadband F-K). Note the excellent consistency.

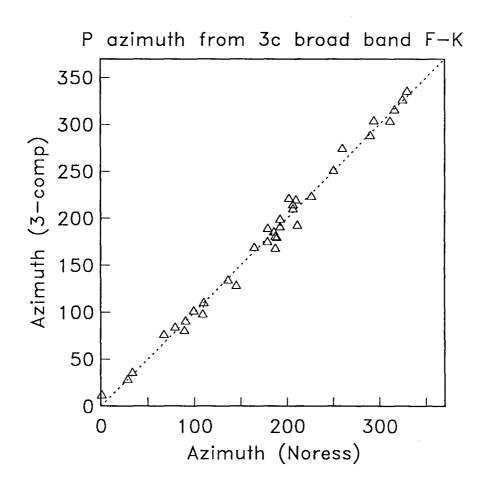


Fig. 7.5.5. Comparison of estimated azimuths of P phases using the full NORESS array (broadband F-K) and the A0 3-component system (polarization analysis). Note that the consistency is similar to that of Fig. 7.5.4.

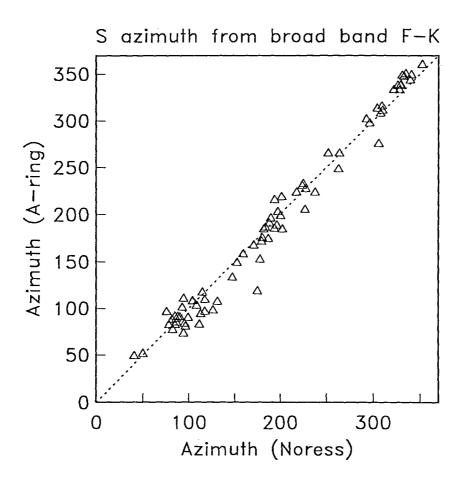


Fig. 7.5.6. NORESS and A-ring azimuth comparison for S phases. Note that the consistency is as good as for P phases (in Fig. 7.5.4).

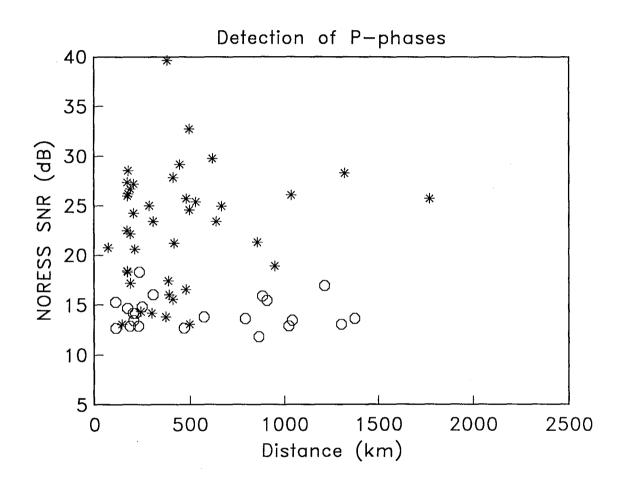


Fig. 7.5.7. Illustration of P-phase detectability of the A-ring SPZ array combined with the 3-component A0 system. P-phases detected by the A-ring SPZ/3-component system are marked as asterisks, whereas nondetected phases are marked as circles. Note that the reference array (NORESS) is clearly superior at distances > 500 km.

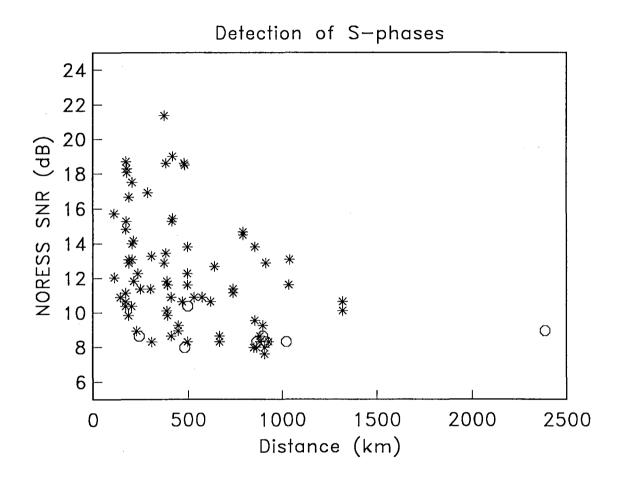


Fig. 7.5.8. Same as Fig. 7.5.7, but for S phases. Note that in this case the small array/3-component system comes close to matching the full array performance.

7.6 Development of two three-component stations in Poland

Background

A network of four regional arrays currently contributes data to the NOR-SAR Data Processing Center in Norway. These arrays are the NORESS and ARCESS arrays in Norway, the FINESA array in Finland and the GERESS array in the Federal Republic of Germany (see Fig. 7.6.1). Data from ARCESS and NORESS are processed jointly in the Intelligent Monitoring System (IMS) that has been installed at NORSAR this year. A forthcoming upgrade of IMS will allow joint processing of data from N arrays and M single stations.

As a cooperative effort between Poland and the United States, two modern seismic stations, including workstations for on-site data recording and analysis, are now being installed in Poland. Each installation comprises a three-component broad band station and a three-component short period station. These stations represent a valuable extension of the existing network of regional arrays in northeastern Europe. In order for IMS, however, to take full advantage of these new stations, the data from Poland must be transmitted continuously and in real time to Norway. This contribution gives descriptions of the field systems installed in Poland, the communications arrangements between Poland and Norway, and the system configured at NORSAR for the purpose of acquiring the data from the two stations in Poland.

Installations in Poland

The two stations in Poland are located at Ksiaz, in the vicinity of the town of Walbrzych in southwestern Poland, and at Stary Folwark, near the town of Augustow in northeastern Poland (see Fig. 7.6.1).

Teledyne Geotech installed in June this year a seismic system at Ksiaz, comprising a short period three-component station (GS-13 sensors), a broad band three-component station (BB-13 sensors), an RDAS-200 data acquisition unit, and a SUN-2 based NOMAD workstation for local data analysis and archiving. Ksiaz is an existing seismological observatory affiliated with the Department of Seismology of the Institute of Geophysics (in Warsaw) of the Polish Academy of Sciences. The local staff at the observatory at Ksiaz will operate the new station and use the workstation in their daily data analysis.

The new station in Stary Folwark will be installed by Teledyne in November. It will be identical to the station at Ksiaz, except there will be no workstation, since there will be no local seismological staff.

Communications links

Reliable communications links between the NORSAR Data Processing Center in Norway and the two sites in Poland can only be accomplished via satellite. Discussions were conducted with the telecommunication authorities in both Poland and Norway in order to determine how such links could be established, and the Polish PTT responded that they would allow the Norwegian Telecommunication Administration (NTA) to deliver and put into operation the ground station equipment needed in Poland.

NTA decided to use the EUTELSAT SMS system for the satellite links between Poland and Norway, and communications were installed in October/November as depicted in Fig. 7.6.2. The data transmission links each have a capacity of 64 kbits/s. The link between Stary Folwark and NORSAR is simplex, while the Ksiaz-NORSAR link is full duplex. The backlink from NORSAR to Ksiaz provides the staff at the Ksiaz observatory with access to data bases at NORSAR, including Stary Folwark data. The Ksiaz to NOR-SAR link uses a set of multiplexers to enable division of the capacity into several channels, as shown in Fig. 7.6.2. The seismic data from Ksiaz use a 19.2 kbits/s channel, the other 19.2 kbits/s channel will be running the SLIP protocol and used for general purposes, one of the 9.6 kbits/s channels will be used for general terminal access, and two remaining channels (9.6 and 2.4 kbits/s, not shown in Fig. 7.6.2) are spare ones.

Data acquisition and analysis at NORSAR

A data acquisition system to handle the data from the two stations in Poland has been configured at NORSAR, that is essentially identical to the data acquisition systems currently handling the data streams from the regional arrays. As seen in Fig. 7.6.2, the communications interface is NORSAR's BUSC system (see Paulsen *et al*, 1989). Otherwise, the data acquisition system comprises a SUN 3/260 computer with a Floating Point Accelerator, a 1.2 Gb disk drive with controller, an Exabyte tape drive with SCSI controller, and Ethernet. This system will make it possible to present the data from Poland to the IMS in the same way data from the arrays are made available.

The 24 October 1990 nuclear test at Novaya Zemlya was recorded by the new seismic station at Ksiaz, and the recordings for both the short period and the broad band stations are shown in Fig. 7.6.3.

S. Mykkeltveit R. Paulsen

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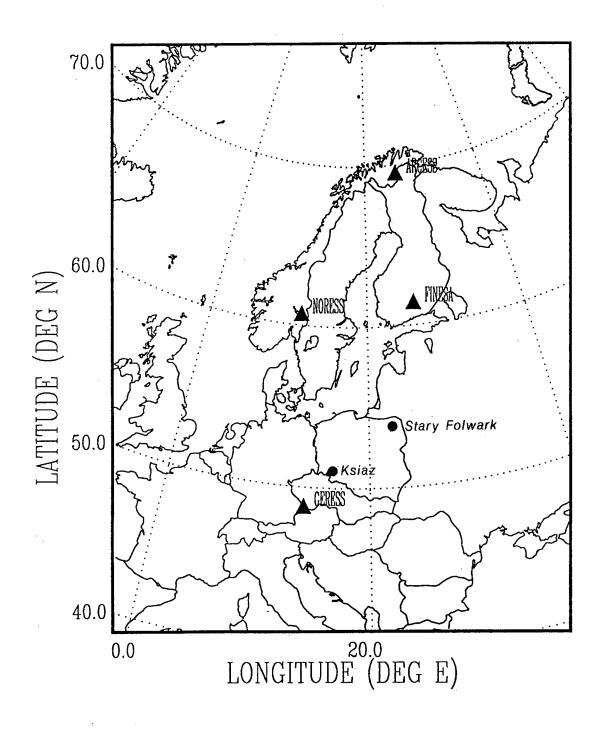
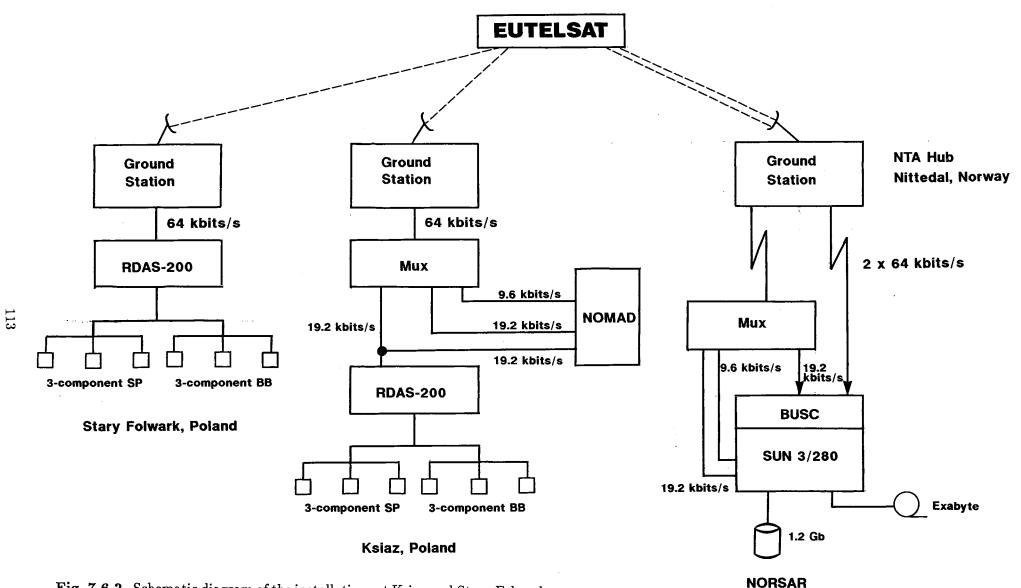


Fig. 7.6.1. The map shows the location of the regional arrays NORESS, ARCESS, FINESA and GERESS, as well as the two new stations in Poland.



Kjeller, Norway

Fig. 7.6.2. Schematic diagram of the installations at Ksiaz and Stary Folwark, the communications links established between these stations and the NORSAR Data Processing Center in Norway, and the NORSAR data acquisition system for the two data streams from Poland.

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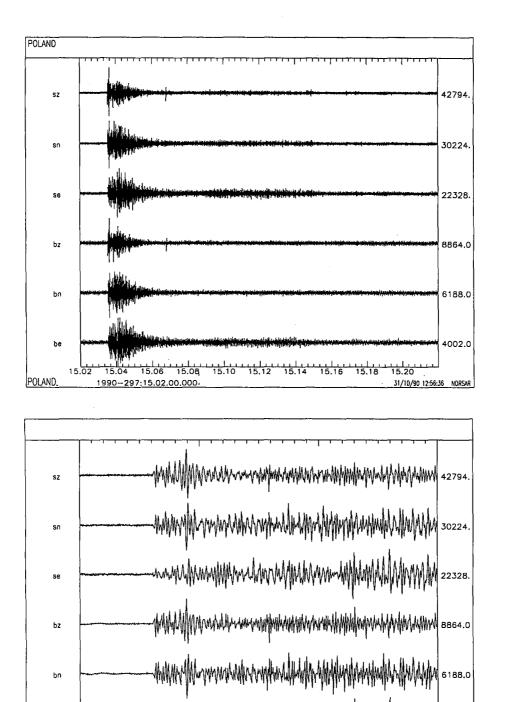


Fig. 7.6.3. Short period (sz, sn, se) and broad band (bz, bn, be) 3-component recording at Ksiaz of the 24 October 1990 nuclear explosion at Novaya Zemlya. The upper frame shows 20 minutes of data, whereas the lower frame covers a one-minute interval around the P onset.

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7.7 Optimal group filtering and noise attenuation for the NORESS and ARCESS arrays

A generalization of Capon's (1970) maximum likelihood technique for detection and estimation of seismic signals has recently been introduced by Kushnir *et al* (1990). By using a multidimensional autoregressive approximation of seismic array noise, a technique to use Capon's multichannel filter for online processing has been developed. Such autoregressive adaptation to the current noise matrix power spectrum has been shown to yield good suppression of coherent noise processes. This paper presents further results of our studies of of adaptive optimal group filtering (AOGF) which now has been applied to more than 80 earthquake and underground nuclear explosion recordings at the small aperture arrays NORESS and ARCESS in Norway (Fig. 7.7.1).

Compared to conventional beamforming, AOGF is demonstrated to provide high signal-to-noise ratio (SNR) gains (12–18 dB) over a wide frequency band (0.2–5.0 Hz), while retaining an undistorted signal waveform. This gain is mainly due to suppression of noise at low frequencies, where both noise power and noise coherency is greatest.

AOGF has also been tested in combination with statistically optimal algorithms for detection and onset time estimation using the maximum likelihood principle. Here, narrow-band filtering has been applied, selecting the frequency band most appropriate for detecting weak arrivals by conventional beamforming. Even in this case, AOGF provides significant gain in SNR (typically 6–8 dB in the 2–4 Hz band) compared to the array beam.

Description of software used

The conventional technique for array signal processing is based on beamforming, band pass filtering and STA/LTA detection. Beamforming is the statistically optimal procedure under the assumption of independent noise among the M different receivers of the array and in this case it improves power signal-to-noise ratio by a factor of M. For correlated noise this procedure is not optimal in the statistical sense. Bandpass filtering gives additional improvement of SNR, but this procedure, evidently, may reduce available information about the signals. The STA/LTA detector is a simple procedure, but it is sensitive only to variations of recorded power due to signal arrival, and it does not make use of spectral differences between signal and noise. So there is room left for improvement of this technique, and a possibility is to use statistically optimal procedures accounting for noise and signal features.

Now, at NORSAR a technique based on statistically optimal procedures has been tested. This technique is illustrated in Fig. 7.7.2 and consists of adapative optimal group filtering (AOGF) followed by optimal detection (OD) and optimal signal onset time estimation (OE) (see Pisarenko *et al*, 1987). AOGF is based on a Wiener optimal filter with frequency response

$$\vec{H}(\lambda) = \vec{G}^*(\lambda)F^{-1}(\lambda)/\vec{G}^*(\lambda)F^{-1}(\lambda)\vec{G}(\lambda)$$

using the multichannel array record $\vec{X}_t = \vec{S}_t + \vec{\xi}_t$, $\vec{S}_t = \vec{G}_t^* u_t$ for input. The output of this filter Y_t is a scalar. AOGF reduces the noise power to a minimum, using the estimated inverse matrix power spectrum $F^{-1}(\lambda)$ of the array noise $\vec{\xi}_t$. The vector function $\vec{G}(\lambda)$ represents the medium frequency response along the paths from the seismic source to the array sensors, u_t is the scalar signal of the seismic source (waveform). For a homogeneous medium, \vec{G}_t is determined by signal arrival delays at different stations. If AOGF is tuned properly ($\vec{G} = \vec{G}$) and $\vec{\xi} = 0$, then the AOGF output Y_t coincides with the signal waveform u_t . The procedure thus avoids introducing any distortion of the signal. If the noise is uncorrelated ($F(\lambda) = I$) (I - identity matrix) and $\vec{G}(\lambda)$ depends on delays only, then AOGF coincides with beamforming.

The inverse power spectrum matrix $F^{-1}(f)$ is estimated from pure noise preceding the signal by a procedure of adaptation using multichannel autoregressive (AR) modelling. AR estimation of this large size matrix function considerably reduces computations and has experimentally proved to be an excellent procedure for estimating the coherent noise matrix power spectrum.

The optimal detector (OD) (Fig. 7.7.2) is based on autoregressive modelling and moving window detection. In a series of experiments OD proved to exceed STA/LTA results due to optimal accounting of spectral variations in the moving window. The optimal estimator (OE) (Fig. 7.7.2) is a maximum likelihood procedure applied to the time interval around the detection time. It is likewise based on an autoregressive modelling procedure and is sensitive to small variations of spectra in a chosen time interval.

Coherency of noise and optimal group filtering

In Kushnir and Lapshin (1984) it is shown that the SNR at the output of OGF tends to infinity with increasing noise coherency. Coherent noise may be represented as a superposition of noise contributions from several spatially distributed sources. ARCESS and NORESS noise seems to have a strong coherent component, which made it possible to achieve power SNR gain factors of AOGF relative to beamforming of about 70–80 at ARCESS and 20–30 at NORESS (Kushnir *et al*, 1990; Kushnir *et al*; 1989). Coherent noise may be recognized from spatial spectral FK-analysis, where noise and signals coming from different sources correspond to different peaks in the slowness vector plane. Strong coherent noise may be represented in the frequency domain as

$$\vec{\xi}(\lambda) = \sum_{k=1}^{N} \xi_k(\lambda) \vec{\phi}_k + \epsilon \vec{\eta}(\lambda), \quad \lambda \in (0, 2\pi]$$

where $\xi_k(\lambda)$ are scalar noise source signals, $\phi(\lambda)$ is the vector frequency response from the k-th noise source to the array receivers, and $\eta(\lambda), k = 1, ..., N$

are independent power spectrum matrices.

$$F(\lambda) = \sum_{k=1}^{N} f_k(\lambda) \vec{\phi}_k(\lambda) \vec{\phi}_k^*(\lambda) + \epsilon^2 \Phi(\lambda)$$
(1)

where $f_k(\lambda)$ is the spectral density of $\xi_k(\lambda)$ and $\Phi(\lambda)$ is the matrix power spectrum of diffuse noise, and $\vec{\phi}_k^*$ is the transposed conjugated vector. It can be seen that if $\epsilon \to 0$, the matrix $F(\lambda)$ projects each vector signal $\vec{Q}(\lambda)$ recorded by the array to the "noise" subspace, i.e., linear subspace

$$\left\{\vec{\phi}_k(\lambda), \ k = 1, \dots, N\right\}:$$

$$f(\lambda)\vec{Q}(\lambda) \xrightarrow[\epsilon \to 0]{} \sum_{k=1}^N C_k\vec{\phi}_k(\lambda)$$

and $F^{-1}(\lambda)$ projects $\vec{Q}(\lambda)$ to the orthogonal subspace $\{\phi_k(\lambda)\}_{k=1,\dots,N}^{\perp}$. Hence, the power of each signal, coming from the "noise" subspace, will be greatly reduced by OGF. We would like to note that compensation of noise by OGF does not require stationarity of the noise source signals $\xi_k(\lambda)$, but stationarity of $\vec{\phi}(\lambda)$ is important.

Description of experiments

Checking of noise attenuation stability. This paper is the second report concerning our attempts to use AOGF at NORSAR. In the first one (Kushnir et al, 1989), we described theoretical capabilities of AOGF and its successful application for broad band extraction of one of the smallest nuclear explosion signals recorded at ARCESS. But in the case described in Kushnir et al (1989), adaptation was done just before the onset time. Therefore some doubts remained as to whether AOGF would work continuously without losing its good features during long periods of filtering time. To check the AOGF performance stability, we applied AOGF to some long-term records of pure ARCESS and NORESS noise.

In Fig. 7.7.3 we show the results of filtering by AOGF the 25 channels of a 40- minute long NORESS noise record. Only the first 2 minutes of the time interval were used for adaptation. AOGF output noise power is gradually increasing, but SNR power gain relative to the beam does not become less than 20. It means that if a signal arrives during this time interval, its SNR will be enhanced by AOGF at least 20 times better than by the beam. Looking at Fig. 7.7.3, one may predict that OGF can work much better than the beam during one hour or even more.

We applied AOGF to 5 ARCESS and 5 NORESS records each consisting of 25 minutes of pure noise, computing the SNR power for each 5 minutes. The results are presented in Fig. 7.7.4. From Fig. 7.7.4b we see that the gain of AOGF relative to beamforming for NORESS is between 15 and 25, for ARCESS from 30 to 75. Again, adaptation is done during the first 2 minutes, and that is why we have the largest gain for the first 5 minutes, including the interval of adaptation. AOGF includes two stages: adaptation and filtering. The first is time consuming, the second is not. If readaptation is only needed once an hour or so, one may attempt to use several AOGFs, tuned to different azimuths and apparent velocities in the same manner as done by beamforming at NORSAR, and this may be more effective for noise suppression in online processing. An illustration of such an application of AOGF is shown in Fig. 7.7.5, where the gain of AOGF is presented versus azimuth. The velocity is constant and equal to 13 km/sec. The peak of the gain corresponds to the southern direction.

Extraction of missed phases. The capability of AOGF to work for a long time without readaptation also makes it possible, using pure noise before P arrivals for adaptation, to enhance the SNR of seismic phases located in time far from the P arrival. Two examples, described below, illustrate the application of all three optimal algorithms: adaptive optimal group filtering, optimal detection, and onset time estimation for extraction of missed seismic phases. It sometimes happens that regional phases like Pn or Lg are missed by the detector applied at NORSAR in the regular processing of NORESS and ARCESS data. We tried to use AOGF, OD and OE to remedy this situation for some of these cases, and they seemed to work well. Two cases were considered.

- a) For case 1 (Fig. 7.7.6a), the Lg phase was detected on NORESS, but the Pn and Sn phases were missed. Fig. 7.7.6b shows data for the same event, as recorded on the FINESA array in Finland. In Fig. 7.7.6c the result of AOGF, OD and OE and beamforming are shown for a window containing the presumed Pn onset. The onset time of the Pn wave is clearly seen, and the maximum of the OE curve is close to the theoretical Pn arrival. (The theoretical Pn arrival time is computed from the event location derived from the FINESA array data.) The theoretical and experimental P arrivals are shown on Fig. 7.7.6a. The first detection shown in Fig. 7.7.6d is questionable (is it caused by the Sn phase from the event considered or not) because the theoretical Sn arrival time differs from the experimental one. The second detection in Fig. 7.7.6d is more likely related to the Sn phase from the event considered.
- b) For case 2 (Fig. 7.7.7a) the regular NORESS processing detected the Pn and Sn phases, but no Lg was detected. This interpretation is confirmed by inspecting the ARCESS records. We have done an adaptation for AOGF just before the Pn arrival. The results are shown in Fig. 7.7.7b, where all three phases Pn, Sn and Lg are evidently detected. Their arrival times are shown on Fig. 7.7.7a as well.

These results suggest possible applications of AOGF in combination with

OD and OE for improvement of the detection lists generated by NORSAR's regular processing of array data.

Adaptive group filtering of seismic signals

AOGF was applied to the processing of 35 teleseismic earthquakes and 44 nuclear explosion signals recorded at NORESS. Earthquake locations are shown in Fig. 7.7.8. Most of the explosions are located at the Shagan River site. This selection of events was made with a view to future work on the discrimination problem. In all the cases, the SNR was much improved by AOGF, but the events may be divided into two classes. One class is where SNR was small in the first place and the other where it was large. In the first class (example in Fig. 7.7.9) improvement of SNR by AOGF is evident, and in the other example (Fig. 7.7.10a) the improvement is not evident in a broad frequency band (0.2–5.0 Hz). But if we consider only the low frequency band (for example, 0.2–0.5 Hz) the advantage of the group filter is seen clearly (Fig. 7.7.10b). This is due to two factors: The first is that at this latter frequency band the SNR is worse for the short-period records used, and the second is that the gain of AOGF seems to be largest due to the high noise coherency in this band.

Conclusion

By application of advanced techniques (apative optimal group filtering, optimal detector, optimal estimator), based on statistical algorithms, processing of NORESS and ARCESS array data may be improved. This improvement could be achieved by taking optimal advantage of array noise coherency and signal frequency contents. Compared to conventional beamforming, AOGF is demonstrated at NORESS and ARCESS to provide SNR gains from 12 to 18 dB over a wide frequency band from 0.2 to 5 Hz, while retaining an undistorted signal waveform. This gain is mainly due to suppression of noise at low frequencies, where both noise power and noise coherency is greatest. But even for the frequency band from 2 to 4 Hz, AOGF provides a typical gain in SNR of the order 6 to 8 dB compared to the array beam. The performance of AOGF appeared to be stable in time without need for readaptation, for time intervals at least one hour long. This may result in possible application of AOGF to supplement conventional beamforming for online signal detection and extraction. The proposed technique may be utilized also in post-processing for detecting and onset time estimating of seismic phases missed by conventional methods. As a result, it may reduce the detection threshold and improve the reliability of event detection and location using array signals.

- A.F. Kushnir, V.I. Pinsky, S. Tsvang, Int. Inst. of Earthquake Prediction Theory, Moscow, USSR
- J. Fyen, S. Mykkeltveit, F. Ringdal, NORSAR

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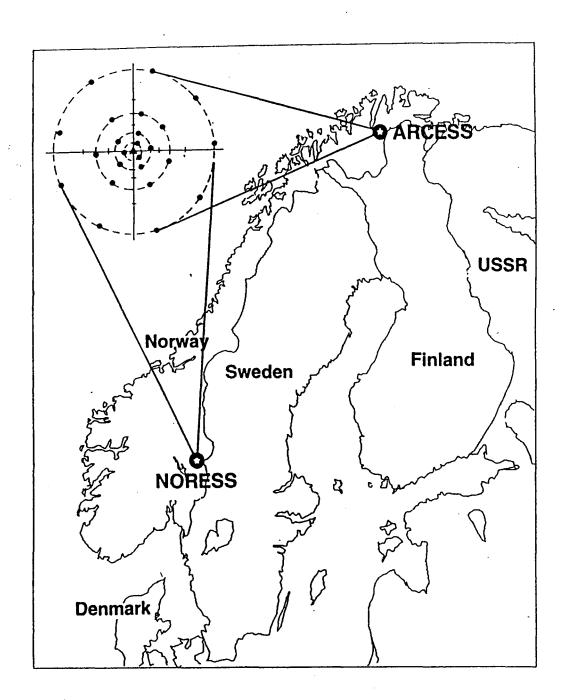


Fig. 7.7.1. The locations and array geometry for the NORESS and ARCESS arrays. The two arrays are essentially identical, each having 24 elements in four concentric rings (A, B, C, D) plus a center element (A0). The diameter of the outer (D) ring is 3.0 km. There are 3-component seismometers at A0 and three of the seven sites in the C-ring.

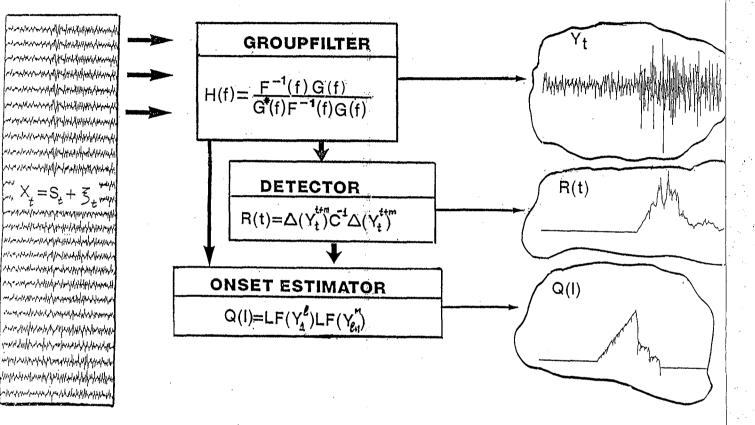


Fig. 7.7.2. Statistically optimal algorithms for preliminary array signal processing. X_t — multichannel seismic record; S_t — signal; ξ_t — noise; $H = H(\lambda)$ — frequency response of OGF; $F^{-1} = F^{-1}(\lambda)$ — inverse matrix power spectrum; $G = G(\lambda)$ — vector medium frequency response; Y_t — scalar output of AOGF, R(t) — detector statistic; Y_t^{t+m} — observations in moving window (width = m samples); Δ — asymptotically sufficient statistics; C^{-1} inverse covariance matrix of Δ computed at adaptation step; $Q(\ell)$ — likelihood function of onset time t_e ; LF — likelihood functions of observations $Y_1^{\ell} = (Y_1, \ldots, Y_{\ell}), Y_{\ell+1}^M = (Y_{\ell+1}, \ldots, Y_M)$.

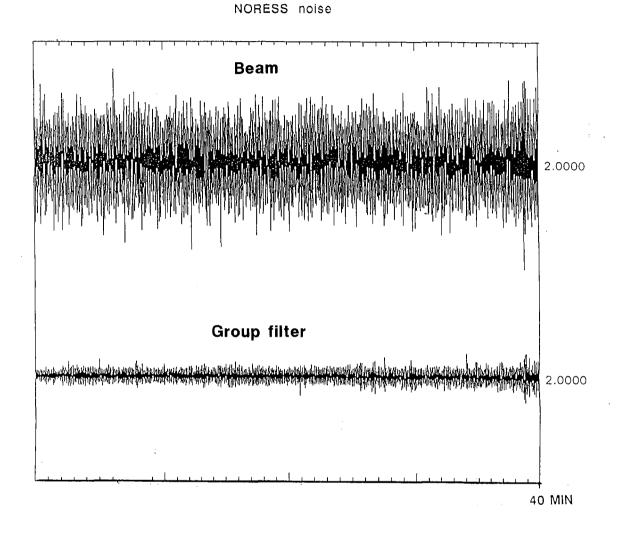
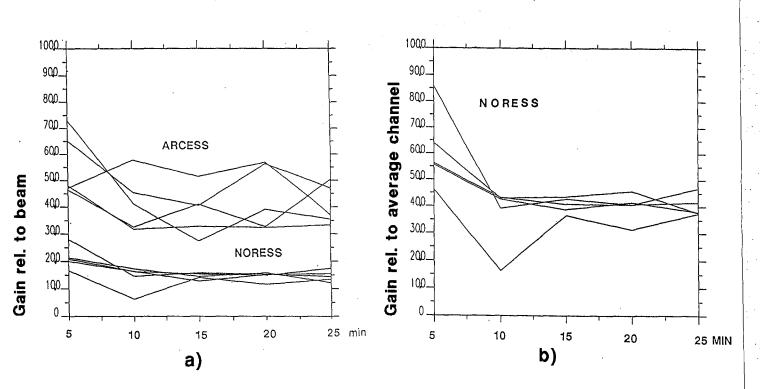


Fig. 7.7.3. 40 minutes of pure NORESS noise filtered by beam and optimal group filter in the same scale.



Gain of optimal group filter

Fig. 7.7.4. Power SNR gain of optimal group filter computed each five minutes: a) relative to beamforming; and b) relative to average NORESS channel.



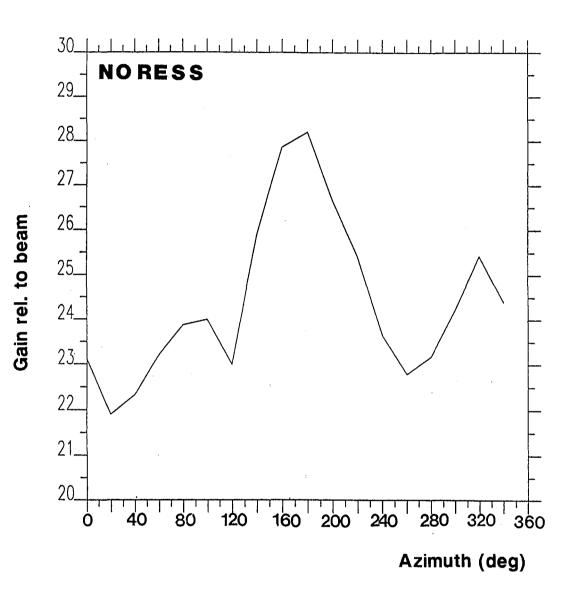


Fig. 7.7.5. Group filter gain for pure noise versus azimuth. The apparent velocity is equal to 13 km/sec. The maximum corresponds to the southern direction.

125

NORESS data. No Pn detection on NORESS. Only Lg detected.

Unossociated	S FKX 3701 beam NV02 at 1990-081:12.37.44.849 snr 4.20
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NV02	
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	Sn ?

Fig. 7.7.6a. Illustration of the AOGF, OD and OE procedures as applied to NORESS data for a small event in Estonia, from which only the Lg phase was detected by the regular processing at NORSAR of NORESS data. The arrows show theoretical and computed (by the OE procedure) arrival times for Pn and Sn phases. Circles mark the time interval, in which there was a search for a Pn phase (see Fig. 7.7.6c), triangles mark the interval for searching for the Sn phase (see Fig. 7.7.6d).

EPX 16100 19 FKX 20181 PF	990-081:12.33.49.812 Lat 59.37 Lon 26.48 Azi 174.42 Dst 231.88 A 2146.3 , 49.87 [0.990 M nose PN at 1990-081:12.34.25.806 vel 7.10 azi 173.30 rpw 0.440 q 3 a 49.87 [4.61 [bond 8	L 2.10 .0 16.0
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FINA2.sz		2513.6
FIN_A3.sz		2427.9
FIN_B1_sz		3919.7
FIN_B2.sz		3702.5
FIN.B3.sz		2946.3
FIN_B4_sz		2293.1
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FINESA	<u>1990–081:12:33.55.800</u> 22/03/90 14:15	09 NORSAR

FINESA DATA.

Fig. 7.7.6b. FINESA recording of the event for which Lg at NORESS is seen in Fig. 7.7.6a.

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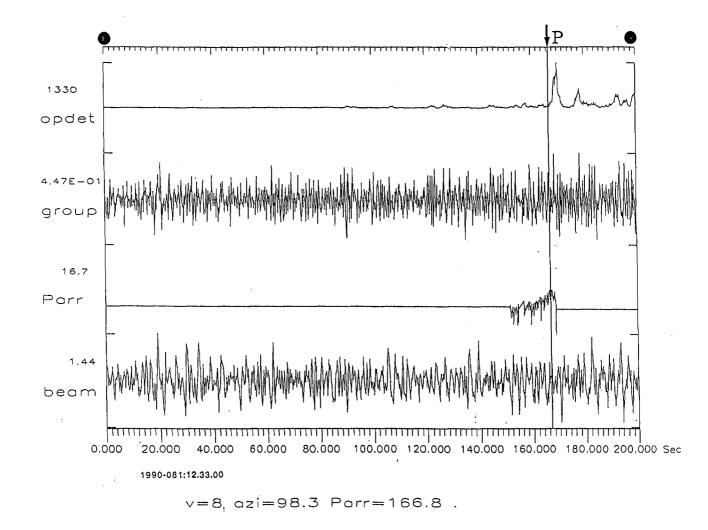


Fig. 7.7.6c. NORESS Pn-wave detection and onset estimation performed on AOGF output data. "V" and "AZI" correspond to apparent velocity and azimuth used in AOGF, "Parr" is computed by OE relative to the beginning of the interval for the search for the Pn phase.

128

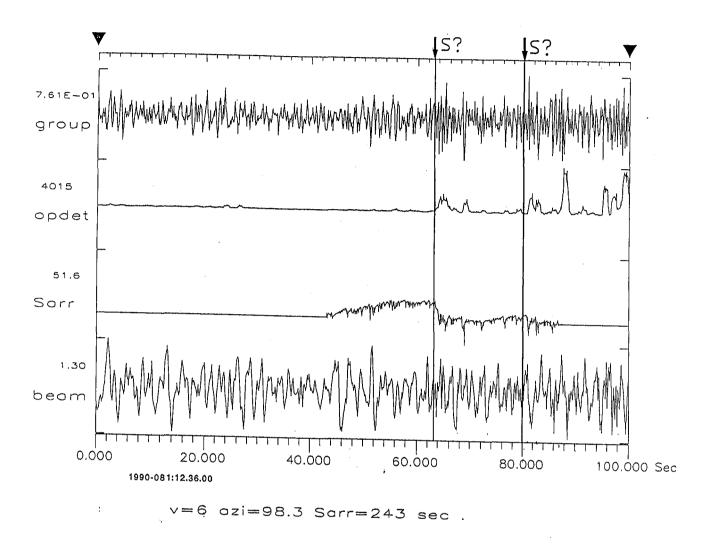


Fig. 7.7.6d. NORESS Sn-wave detection and onset estimation performed on AOGF output data. "V" and "AZI" correspond to apparent velocity and azimuth used in AOGF, "Sarr" is computed by OE relative to the beginning of the interval for the search for the Pn-phase.

		↓Lg	
EPX 56280 19 FKX 6918 Pho	990-101 ose PN c	:09.00.31.166 Lot 64.9 Lon 23.69 Azi 54.63 Dst 721.81 A 567.54 , 0.506 / 3.03 ML 1.9 June 101:09.02.07.135 vel 9.10 ozi 51.80 rpw 0.340 q 1 o 0.506 / 4.12 /bond 3.50	90 5.50
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NORESS	09.0 1990-	09.03 09.04 09.05 09.06 09.07 01:09:01.37.133 5 11/04/90 14:59:	J 35 NORSAR

NORESS data. No Lg detected on NORESS.

Fig. 7.7.7a. Illustration of the AOGF, OD and OE procedures as applied to an event from the USSR/Finland border region, for which the Lg phase was not detected by the NORESS regular processing. (The Sn phase at approximately 09.04 was detected, but incorrectly assigned as Lg.) Arrows show estimates of arrival times, using the OE procedure.

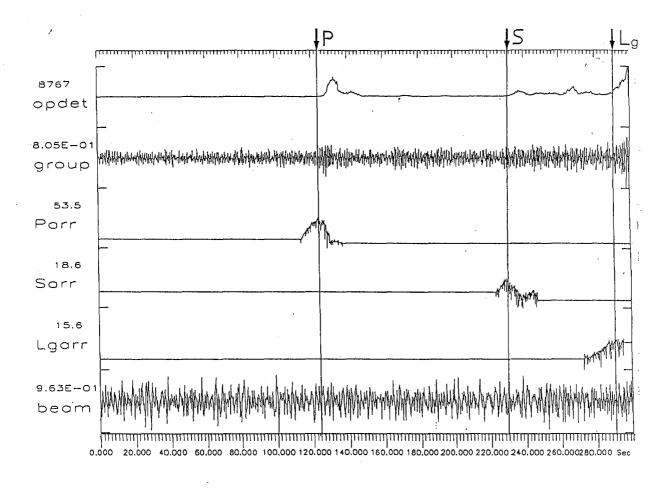
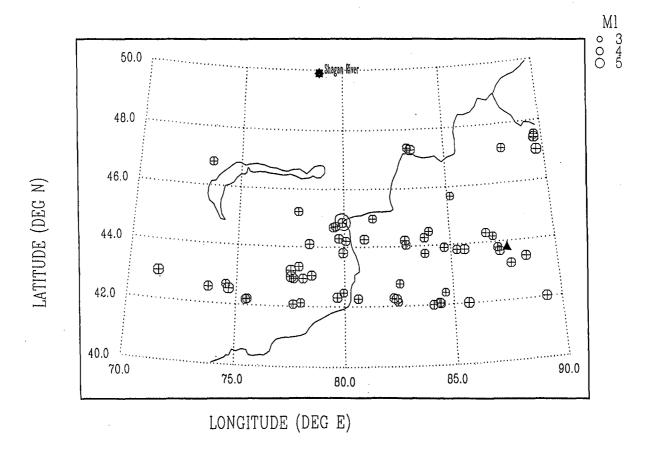


Fig. 7.7.7b. Pn, Sn and Lg detection and estimation performed on AOGF output data. "Time" gives the time of the beginning of the adaptation. "Parr", "Sarr" and "Lgarr" are computed by OE relative to the beginning of the interval.



EARTHQUAKES

Fig. 7.7.8. Map showing the location of 35 earthquakes used in this study. Most explosions used are located at the Shagan River site.

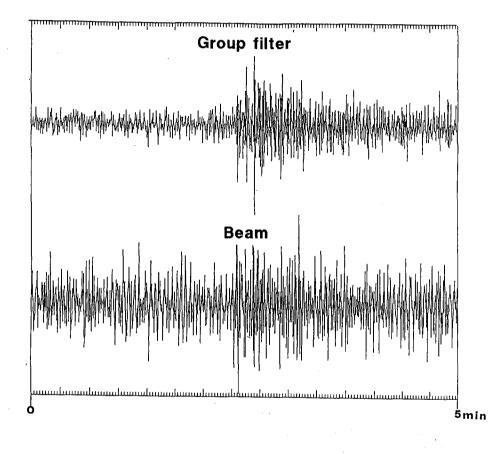


Fig. 7.7.9. Example of earthquake record filtered by beam and AOGF.

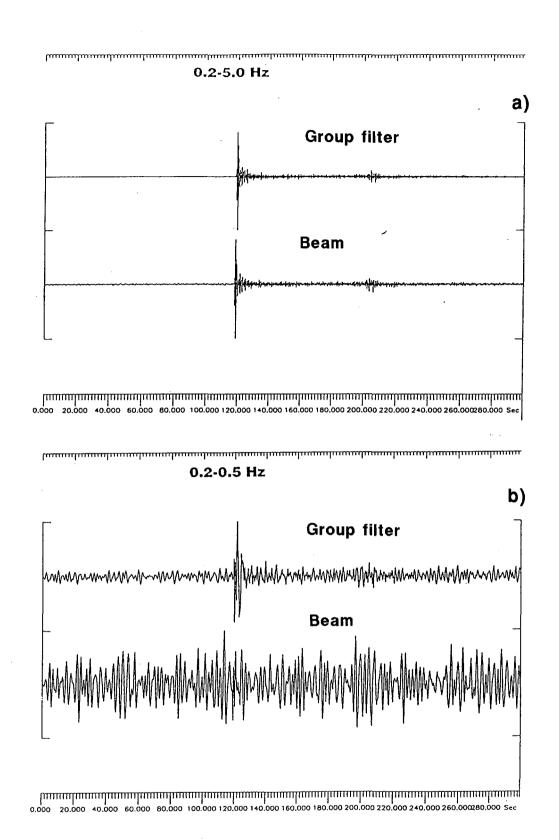


Fig. 7.7.10. Example of nuclear explosion record filtered by beam and AOGF in: a) broad frequency band and b) low frequency band.